

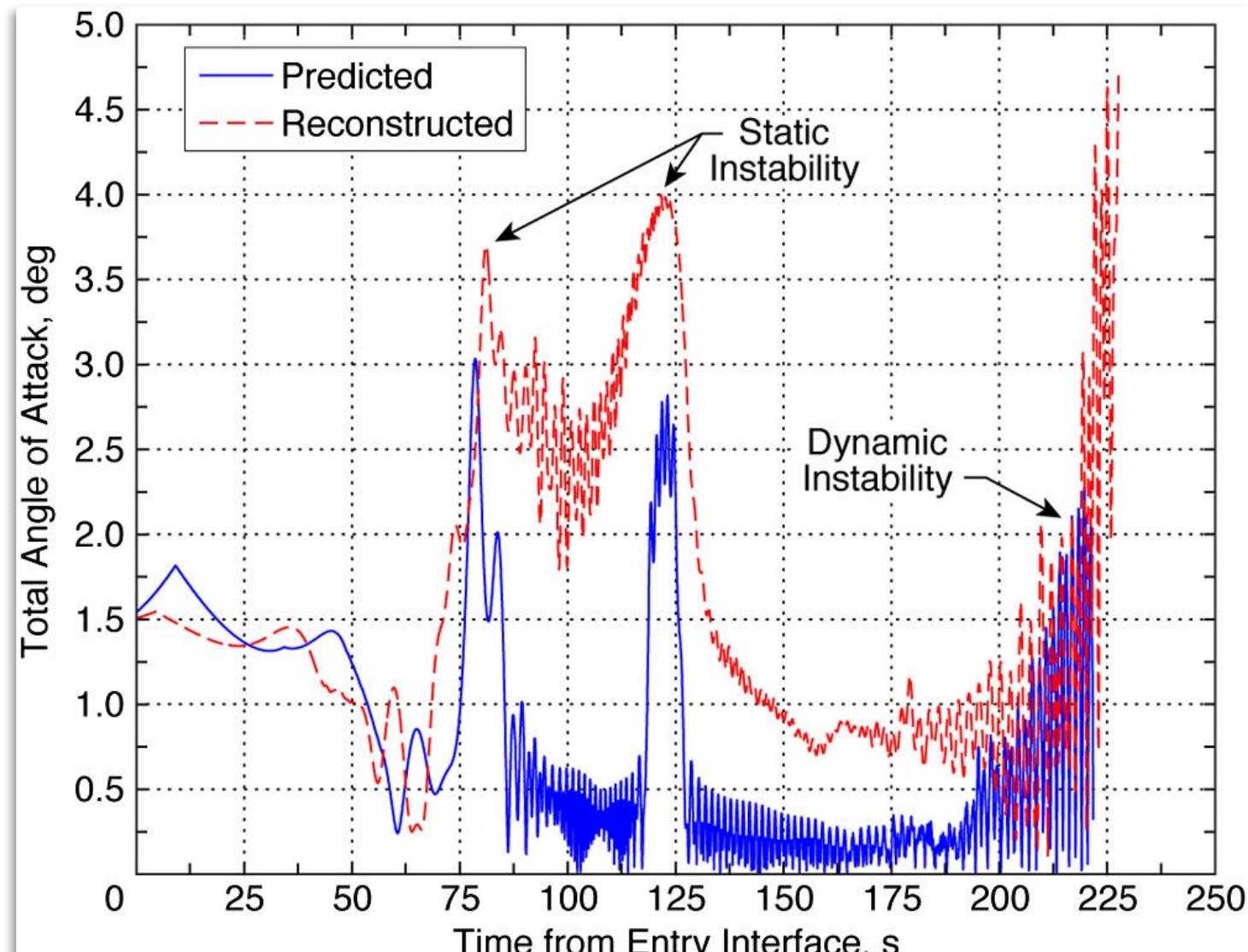
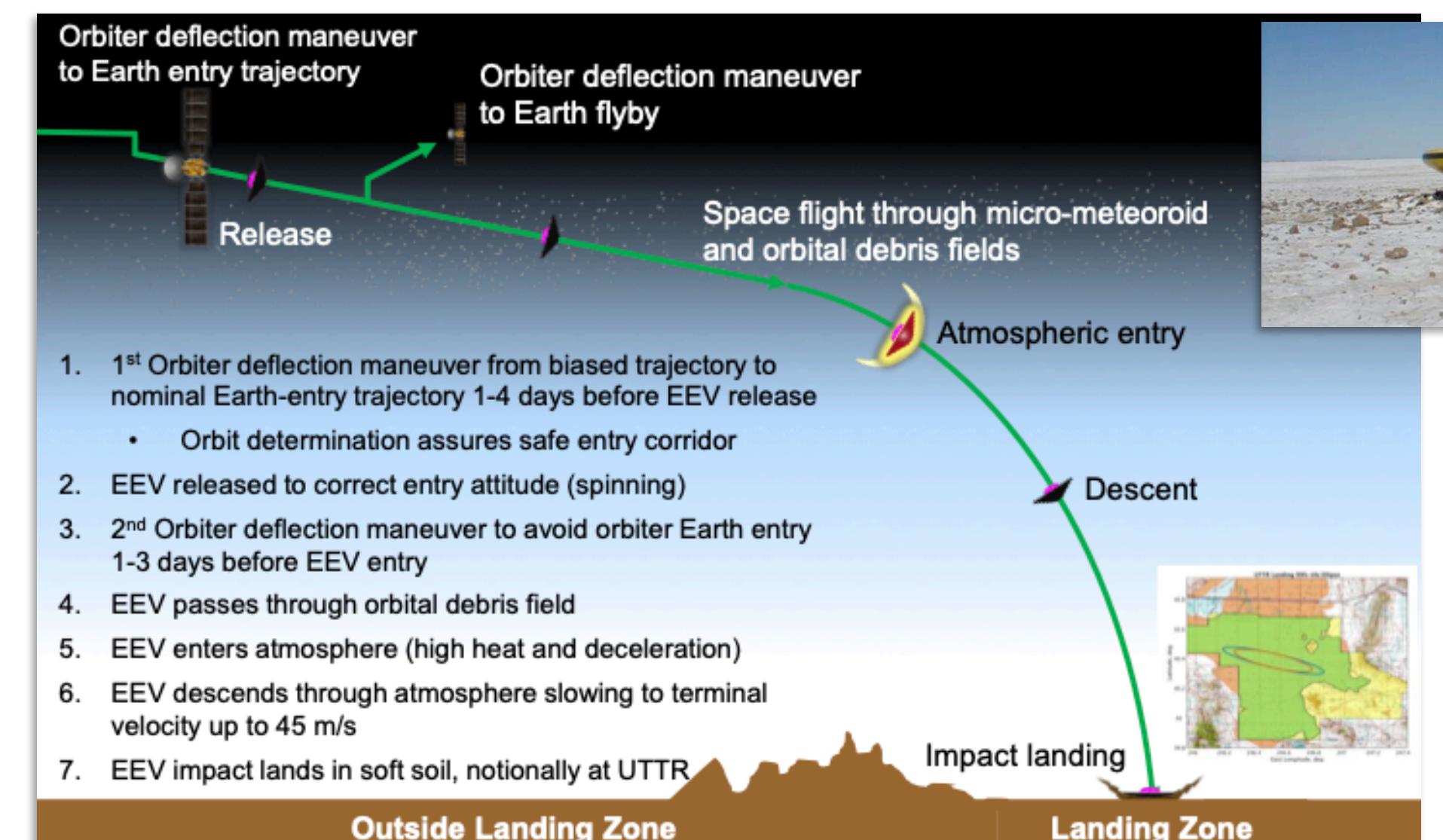
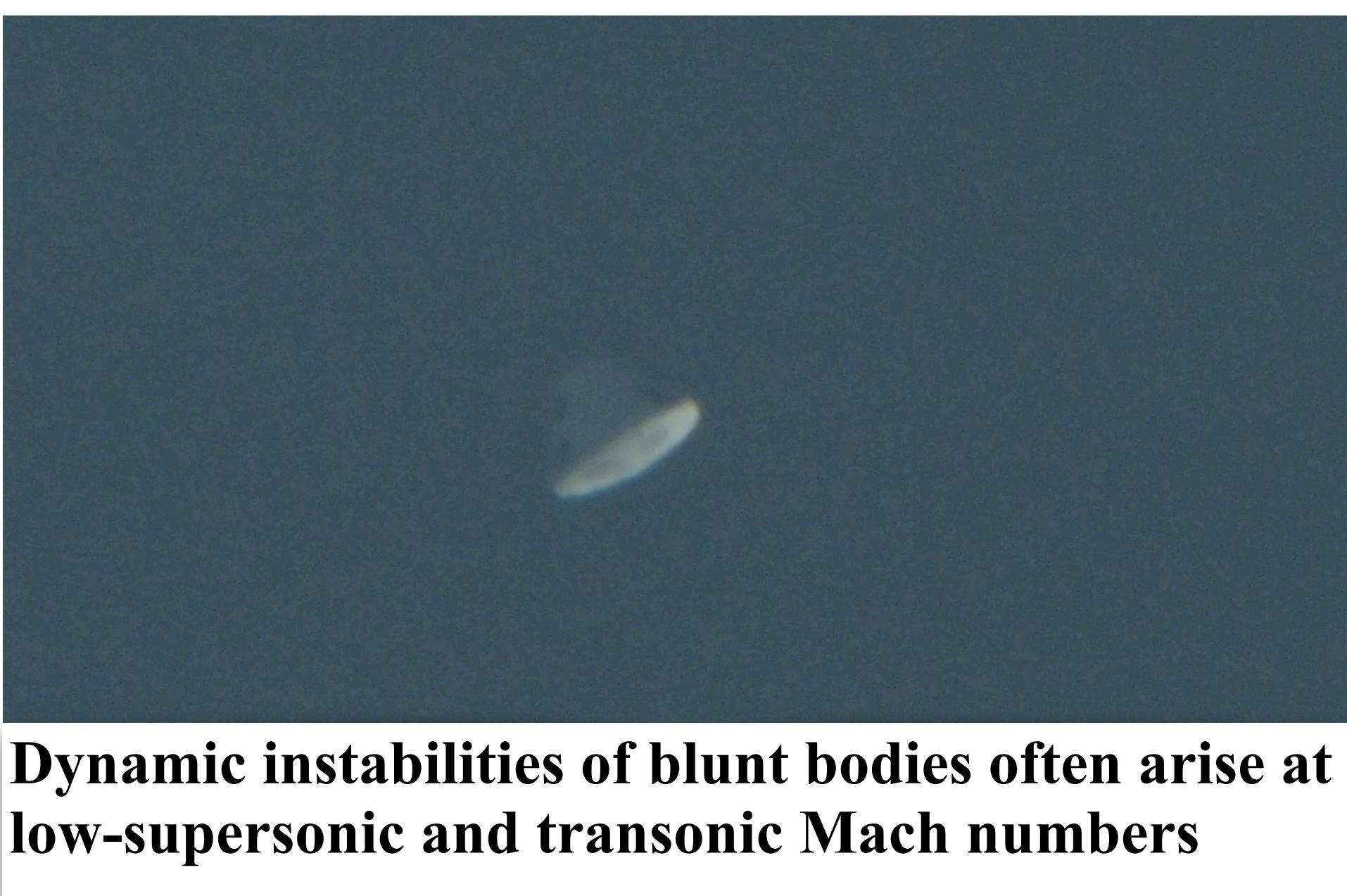


# Dynamic Stability Methodologies and Capabilities

Joseph Brock  
Eric Stern  
Cole Kazemba  
Quincy McKown  
Dirk Ekelschot

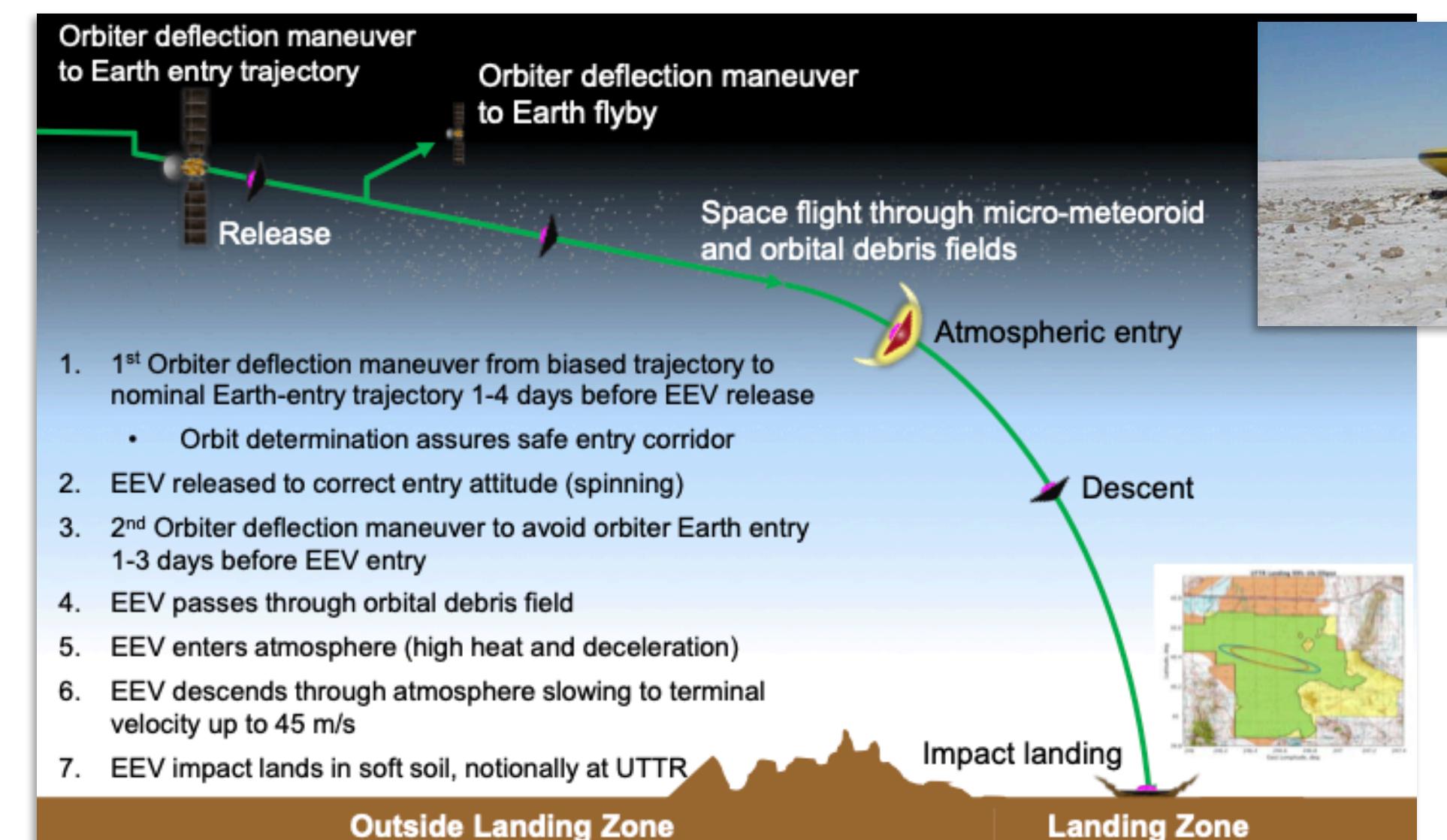
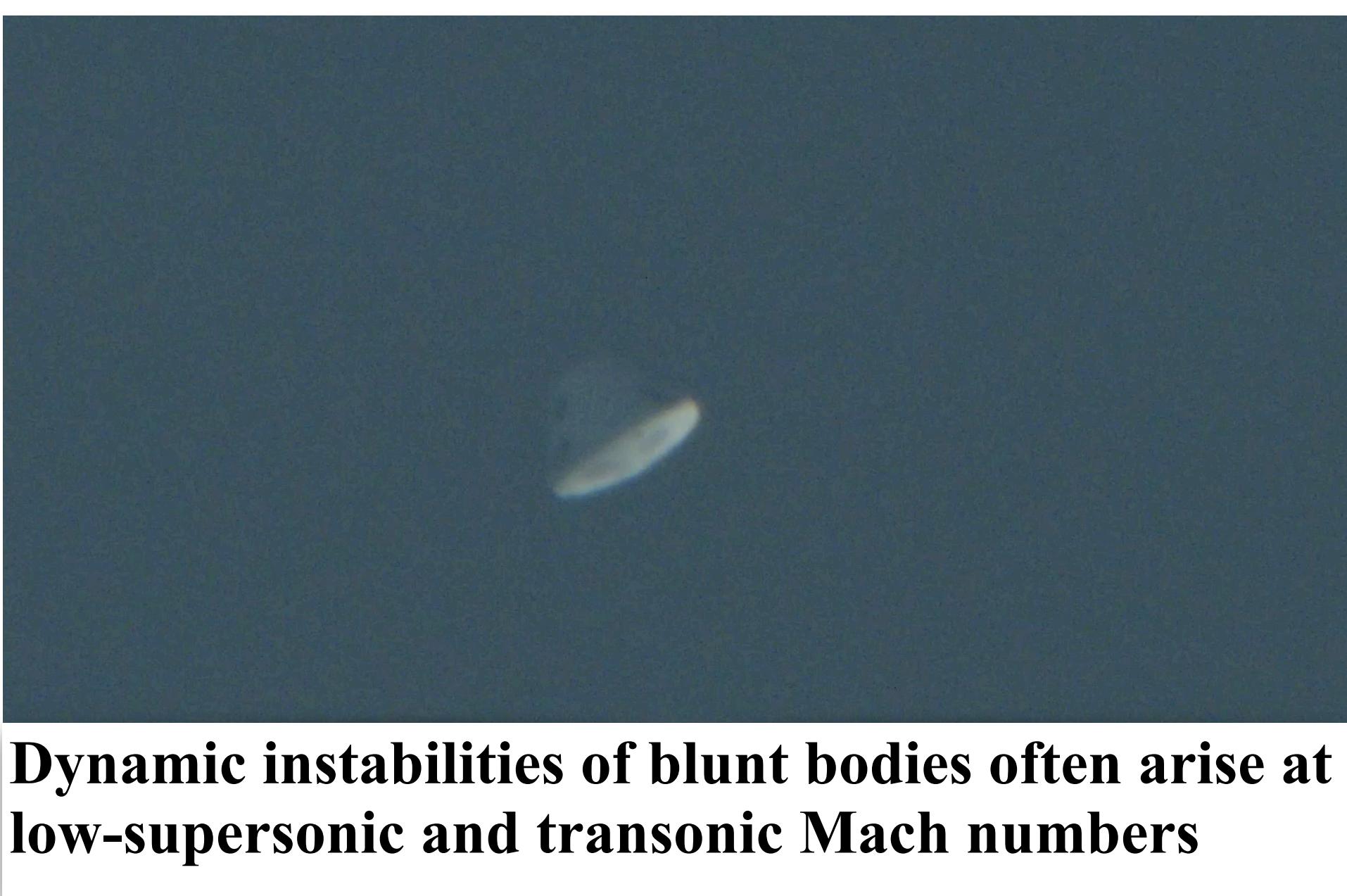
# Characterization of Dynamic Stability

- Blunt-body capsules are subject to dynamic instabilities at low-supersonic and transonic Mach numbers
- Dynamic stability typically characterized exclusively via experiment: forced-, free-oscillation, and ballistic range
  - These methods have a long pedigree of producing dynamic aero for missions
  - However, each method has drawbacks resulting in uncertain predictions
- Current entry missions have dynamics challenges:
  - MSR EES: dynamics during terminal descent drive impact angle which is key for containment
  - Dragonfly: coupled capsule-chute dynamics drive Lander separation event
- Mission needs motivate improved capabilities beyond what standard methods can provide
- Renewed effort on various fronts to characterize dynamics via new testing and computational methods

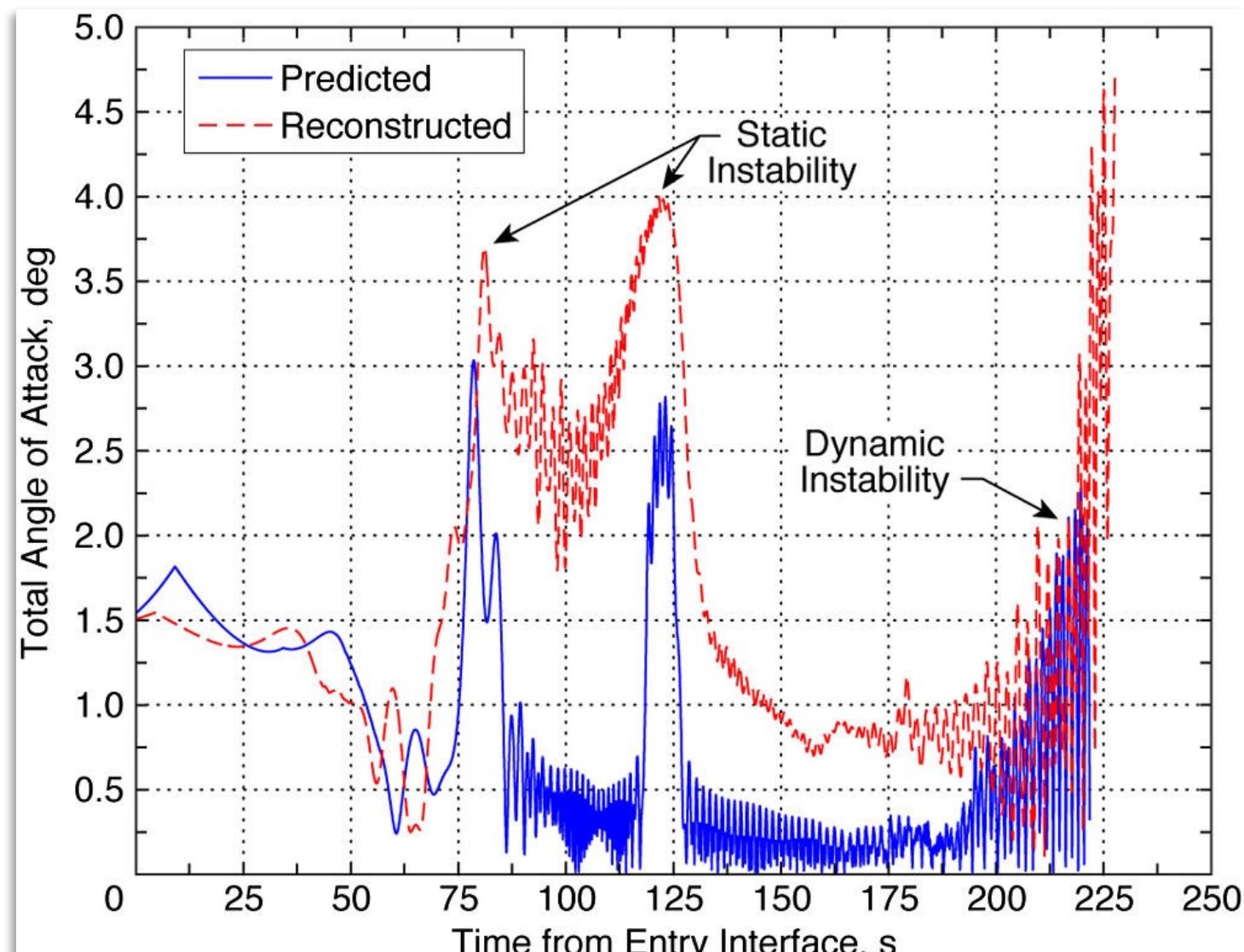


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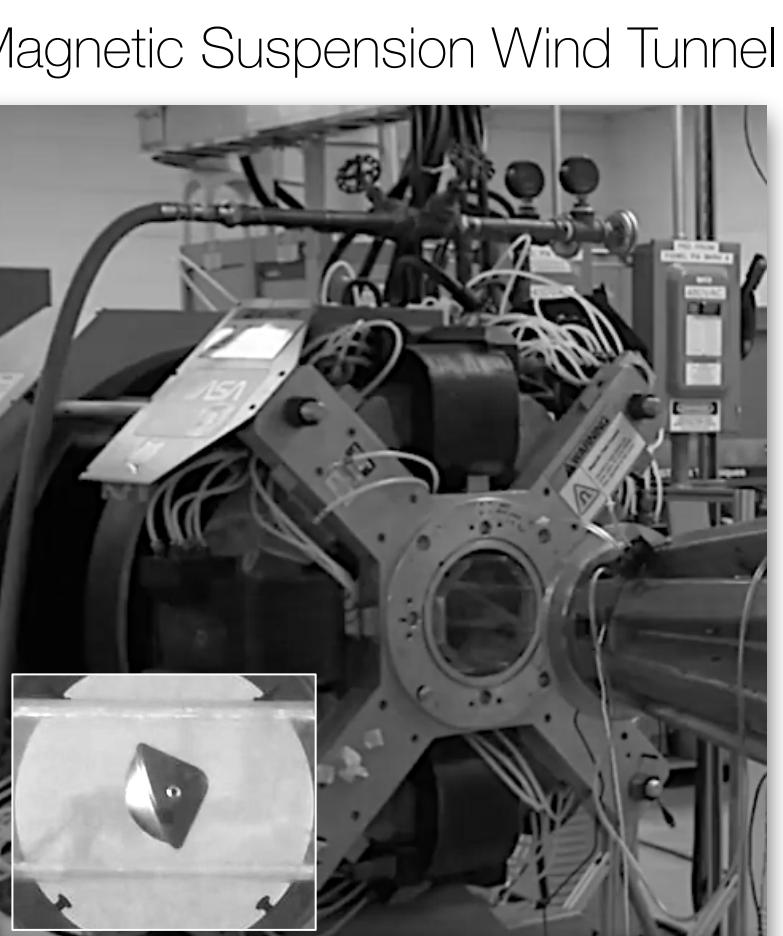
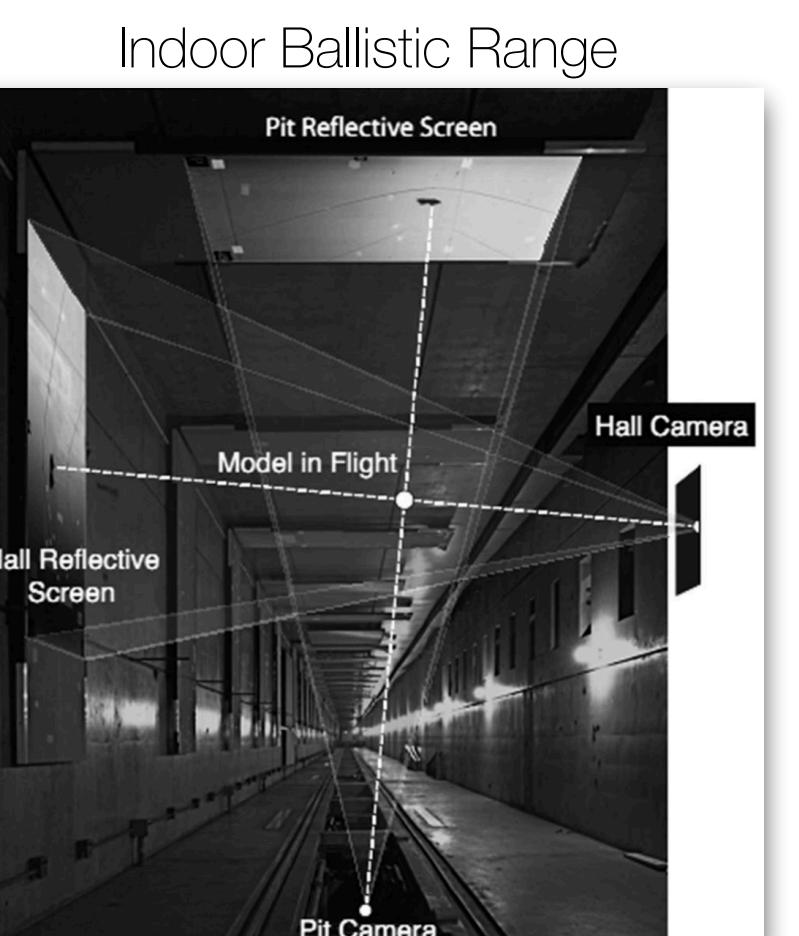
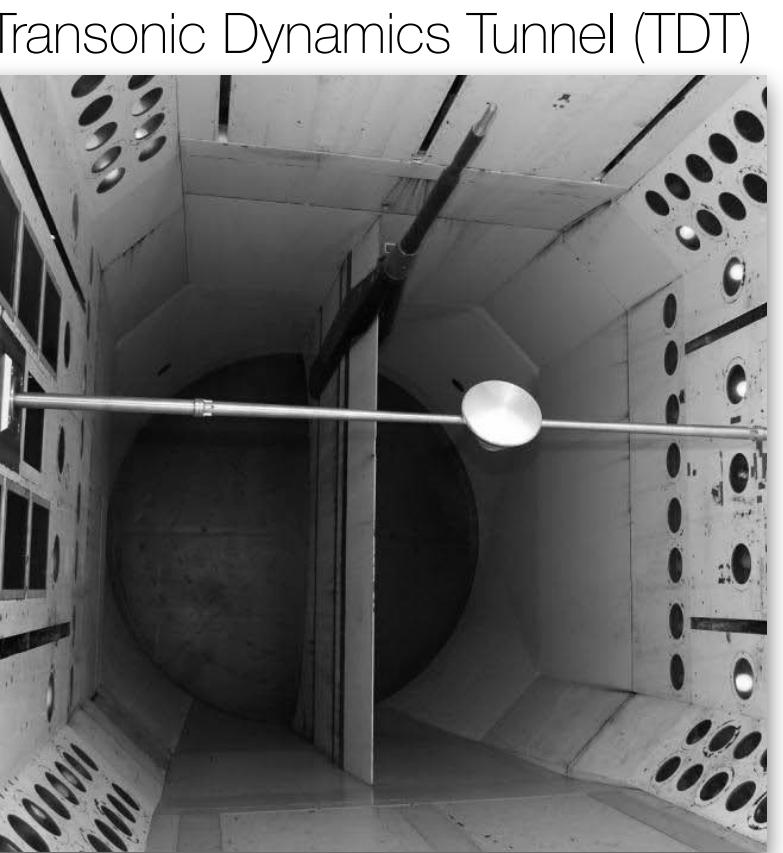
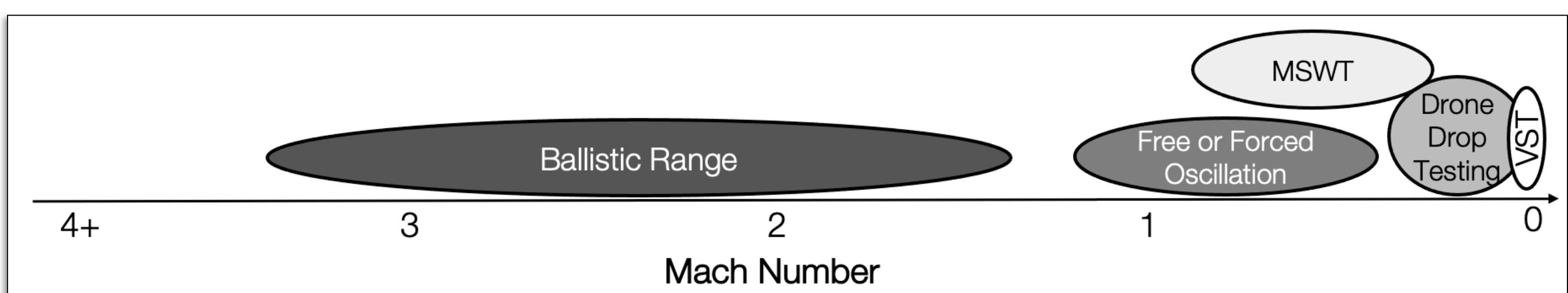


**Mars Phoenix Lander (Desai, 2011)**



# State of the Art: Experimental Facilities

- The current paradigm for dynamic stability testing relies on a piecemeal of different test methods:
  - Multiple test methods provides Mach coverage and helps to compensate for the deficiencies of each individual test method.
  - Flight testing requires typically occurs at lower speeds, sub-scale, or approximate Reynolds number due to gas composition differences
  - Sting mounted setups mirror classic wind-tunnel approaches to provide force and moment data directly
  - Each test methodology relies on a different data reduction approach, all of which differ from flight reconstruction methods
  - Little overlap between the attainable Mach numbers for the different methodologies.
- Each test approach has one or more key weaknesses:
  - Facility induced effects (e.g. stings)
  - Ability to match dynamic similitude and/or Reynolds Number
  - Richness of data for reconstruction and ADB development (e.g. loss of forces/moment data)
- Number of available test facilities is limited:
  - NASA Ames HFFAF and Aberdeen are the only available ballistic range facilities
  - NASA LaRC TDT facility is standard for free- and forced oscillation. Scheduling is difficult
  - Subsonic MWST is coming online to address some of the weakness above



Hypervelocity Free Flight Aerodynamics Facility (HFFAF)

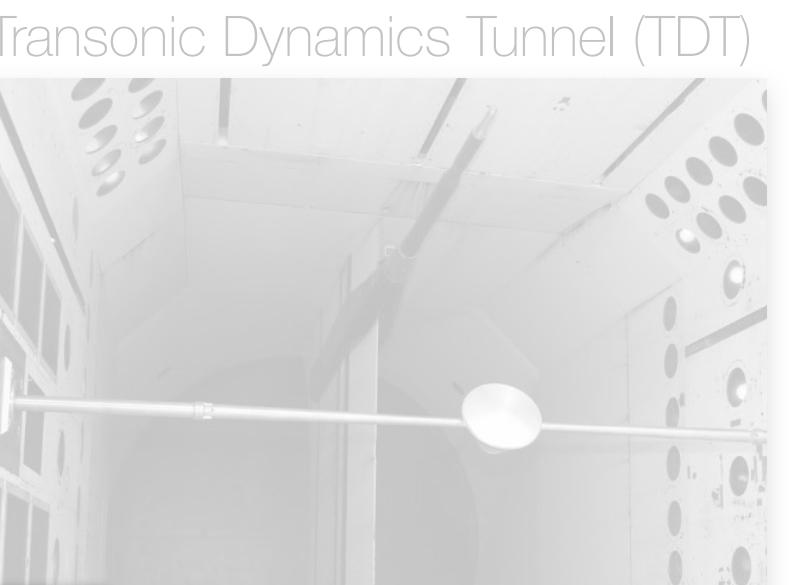


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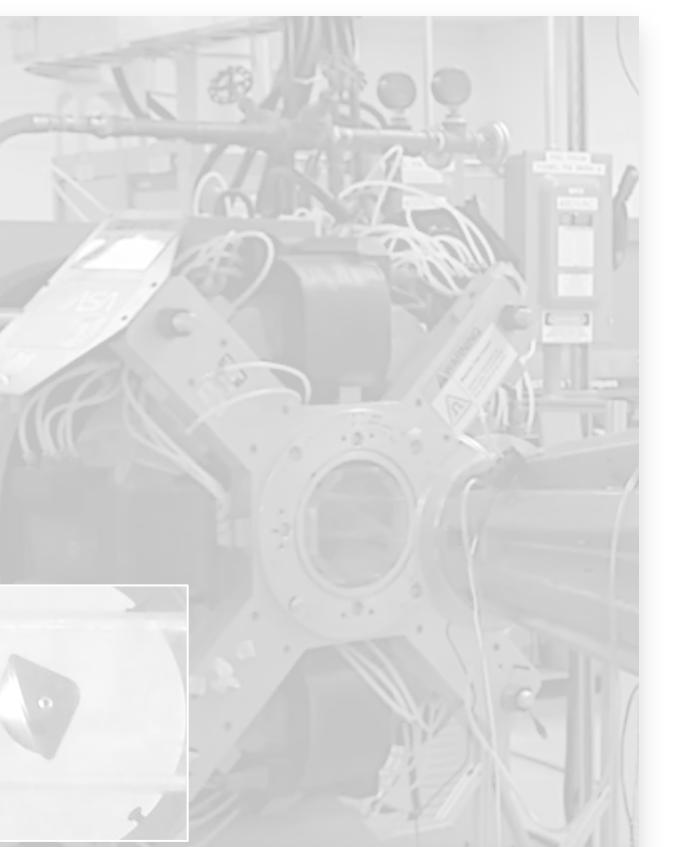
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  - Multiple test methods provides Mach coverage and helps to compensate for the deficiencies of each individual test method.
  - Flight testing requires typically occurs at lower speeds, sub-scale, or approximate Reynolds number due to gas composition differences
  - Sting mounted setups mirror classic wind-tunnel approaches to provide force and moment data directly
  - Each test method requires reconstruction
  - Little overlap between methods
- Each test approach has significant deficiencies
  - Facility induced noise
  - Ability to match initial conditions
  - Richness of data
- Number of available facilities
  - NASA Ames Hypersonic Wind Tunnel
  - NASA LaRC Transonic Dynamics Tunnel
  - Subsonic MWS

There is no test capability that can simultaneously:

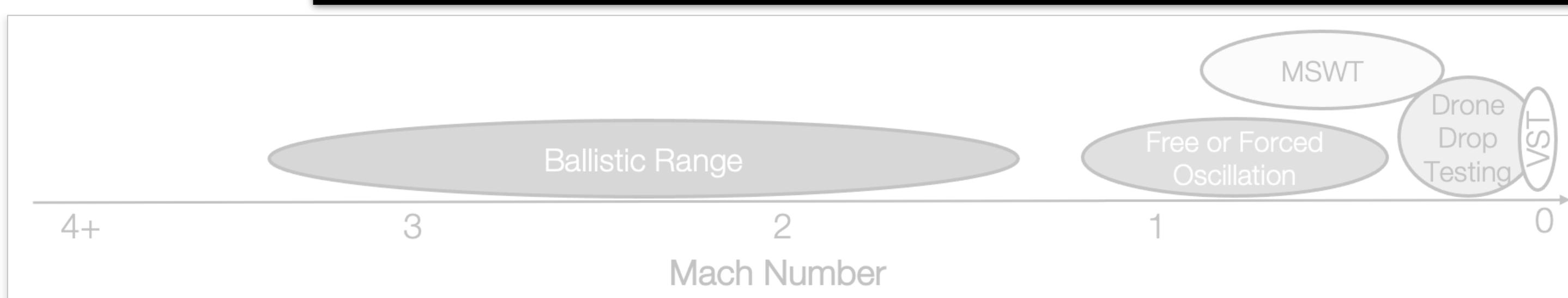
- Replicate a flight-like environment across Mach regime of interest
  - Mach, Re, Degrees of Freedom, Free from interference
  - Free-Flight testing in transonic regime is not possible in current ground facilities
- Provide controlled and understood initial conditions
- Provide a detailed history of the vehicle state
  - Forces and moments, vehicle orientation and rotation rates, surface pressure
- Allow for enough test repeats to generate statistically significant set of observations
  - Oscillatory behavior is driven by interaction with the wake, making it inherently stochastic
  - Each shot in a ballistic range produces few oscillations in  $\alpha_T$



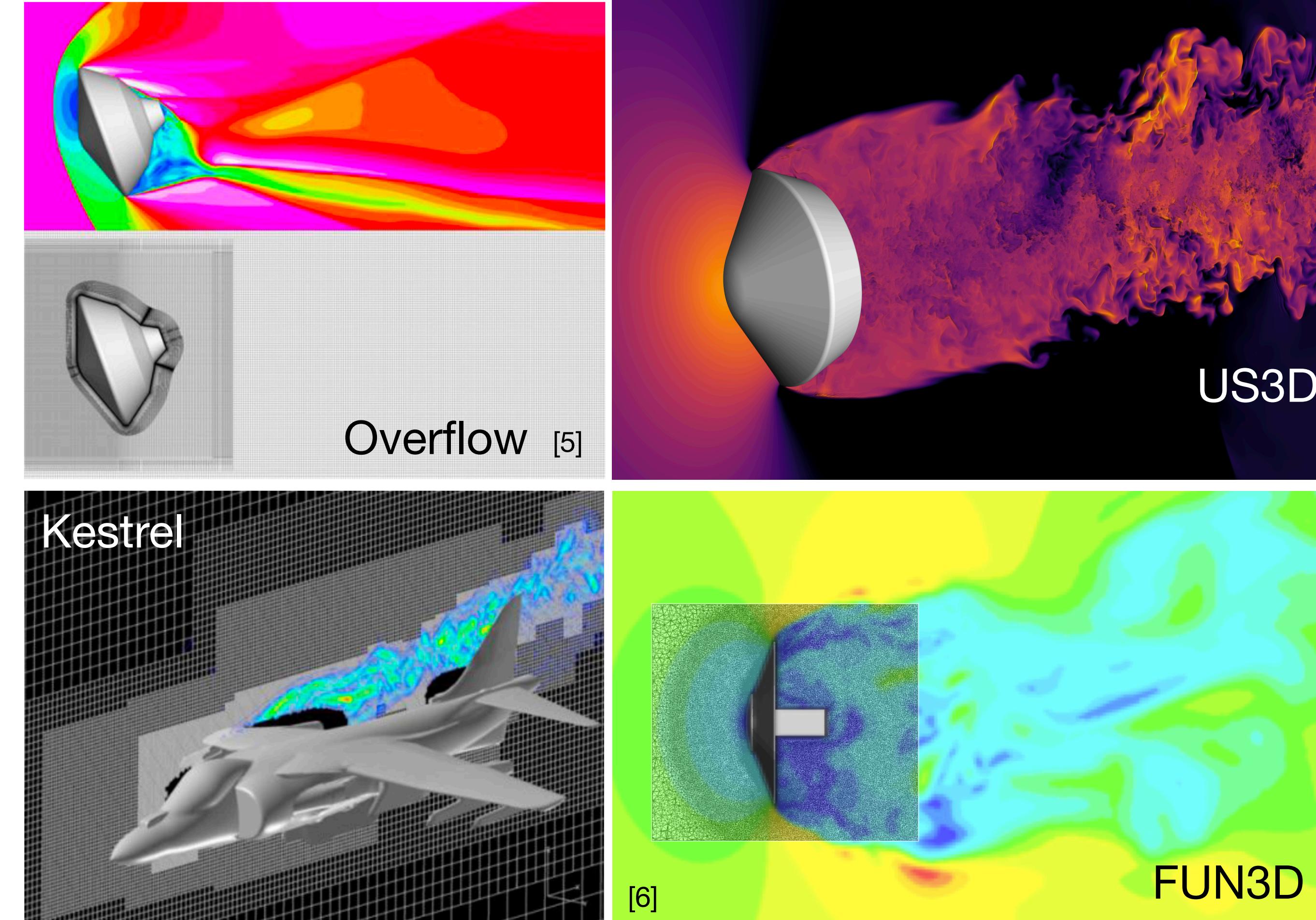
Magnetic Suspension Wind Tunnel



Hypervelocity Free Flight Aerodynamics Facility (HFFAF)

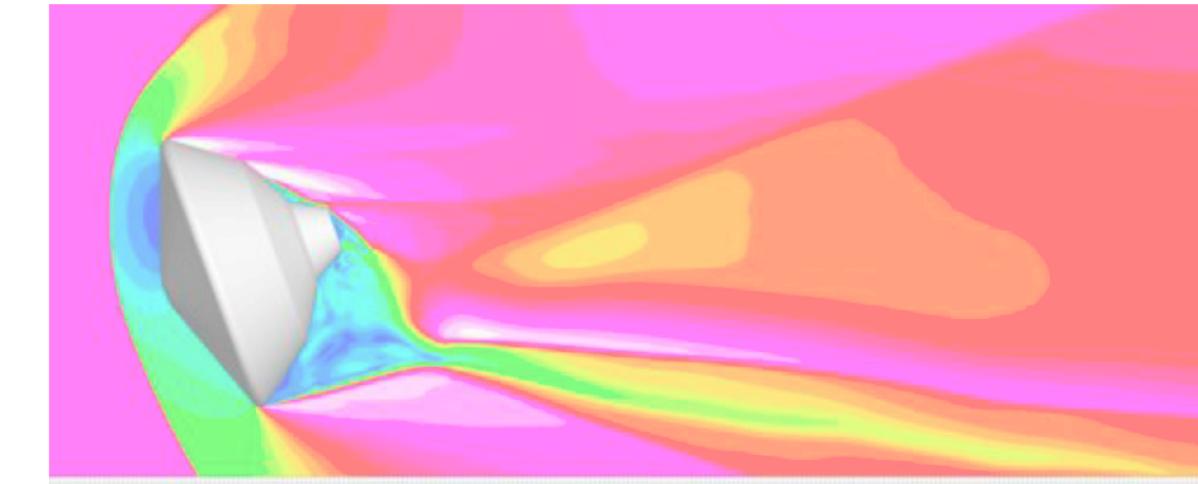
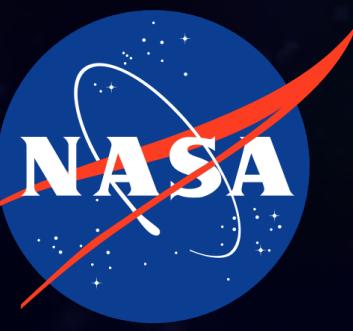


# Computational Capabilities

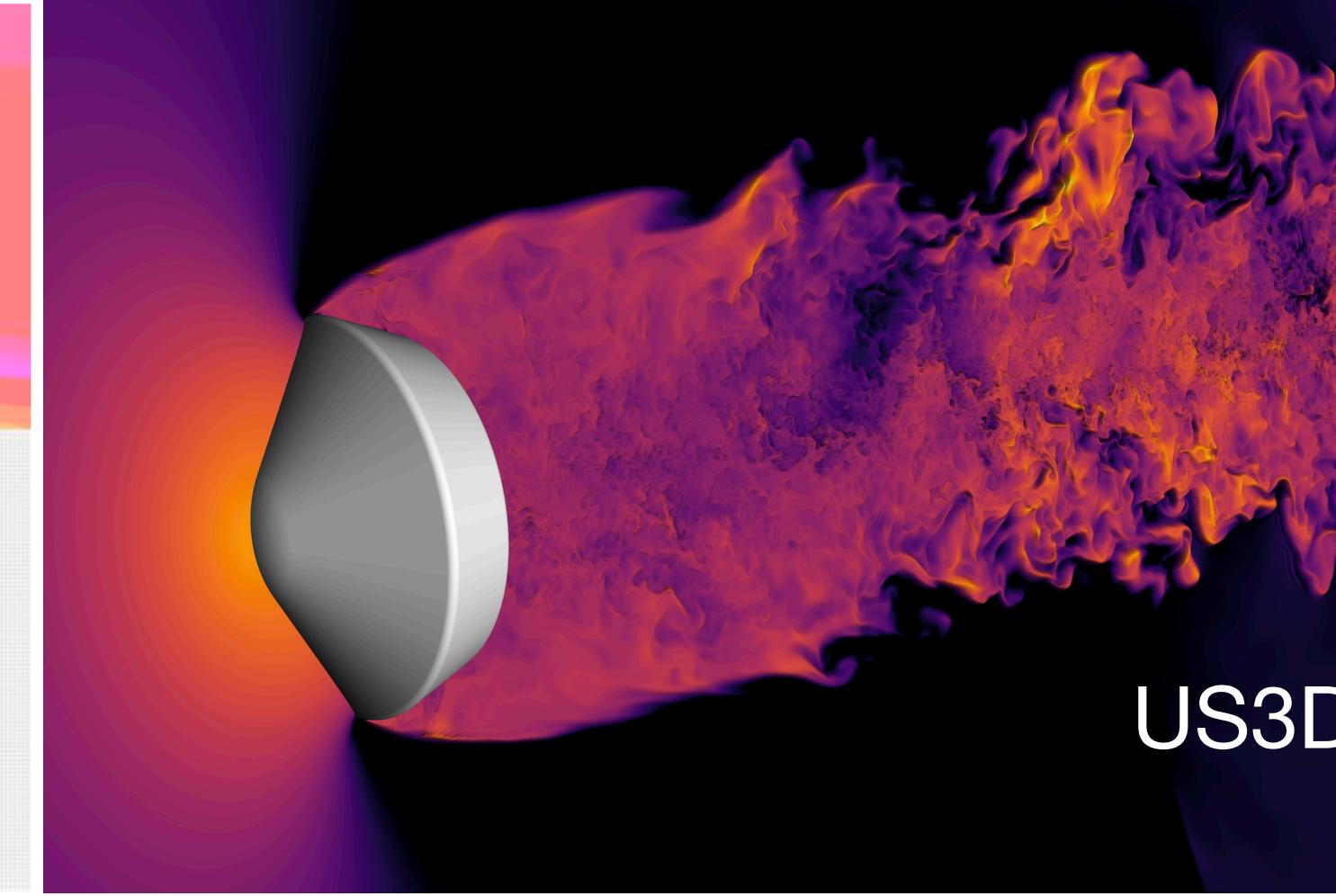


- Inherent constraints in test facilities motivate the development of complementary computational tools
- Several computational codes capable of 6DoF motion are emerging
  - Dynamic motion allows for simulations of forced and free-flying behavior of entry vehicles
- Simulation software verified with experiments will be used to generate dynamic databases anchored with experimental results
- Multiple tool sets provide wide range of Mach numbers and flow regimes to be analyzed

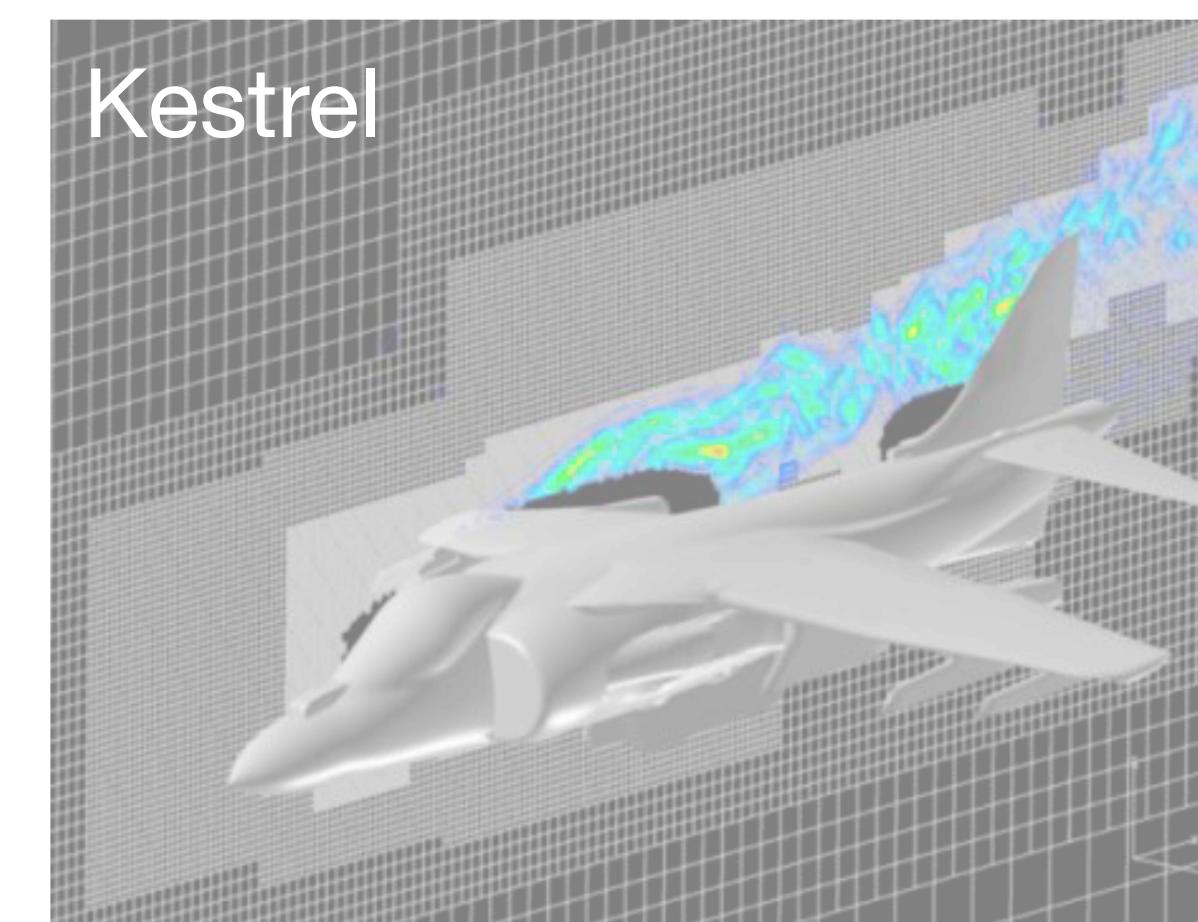
# Computational Capabilities



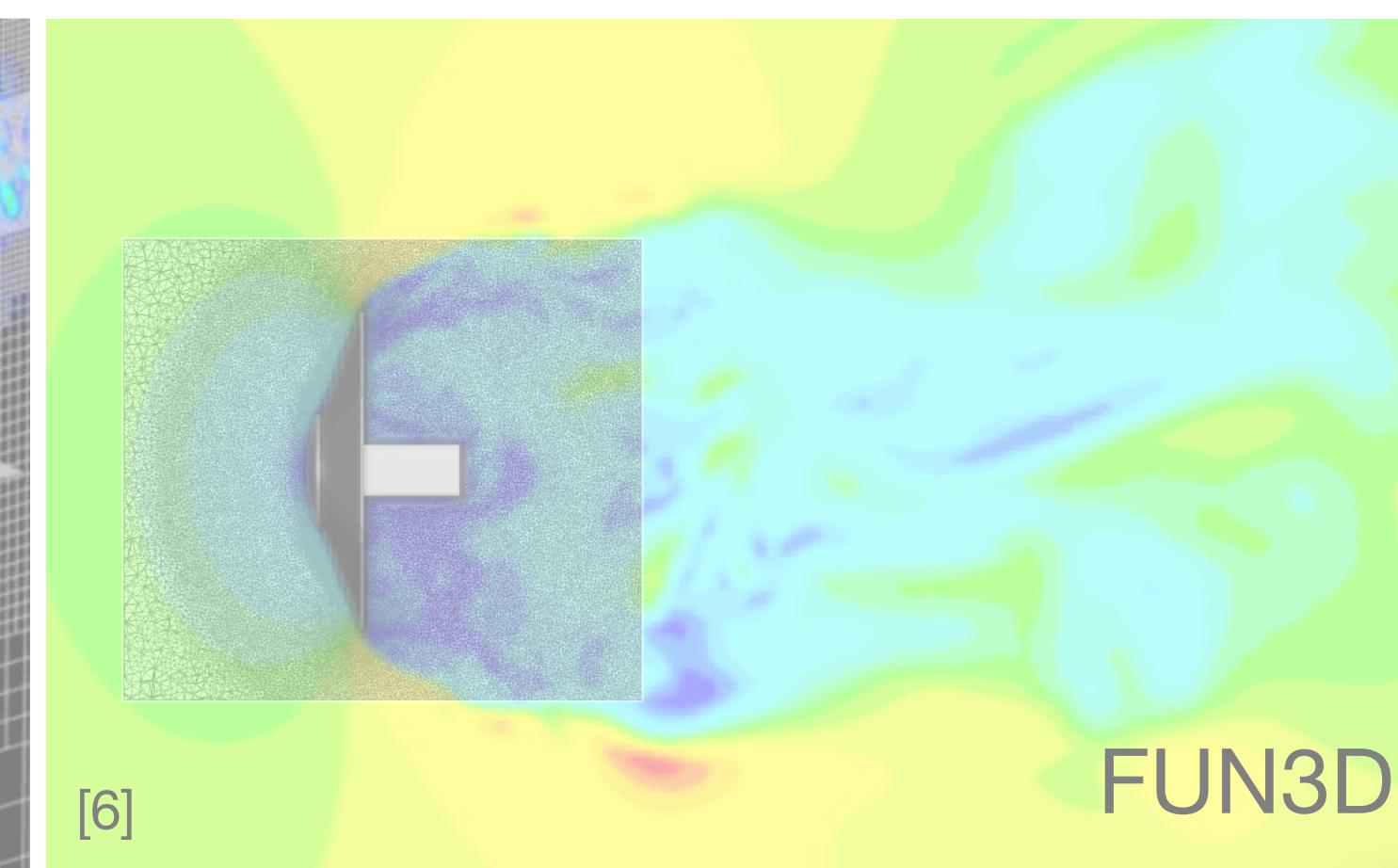
Overflow [5]



US3D

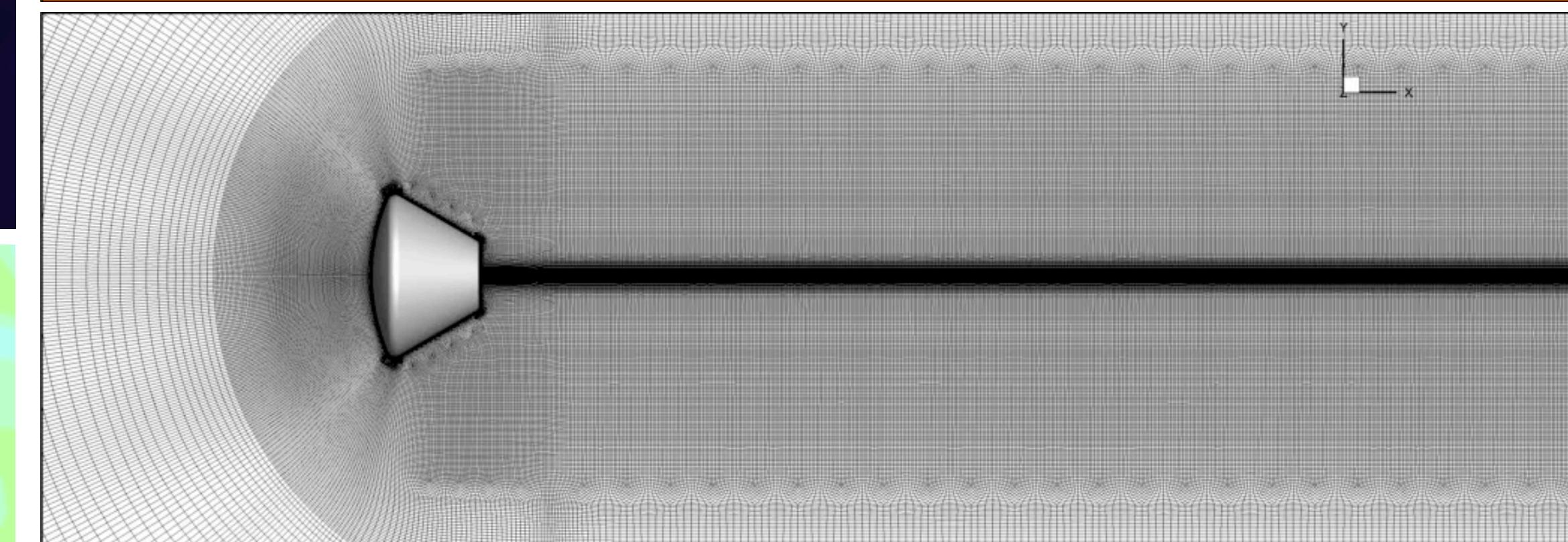
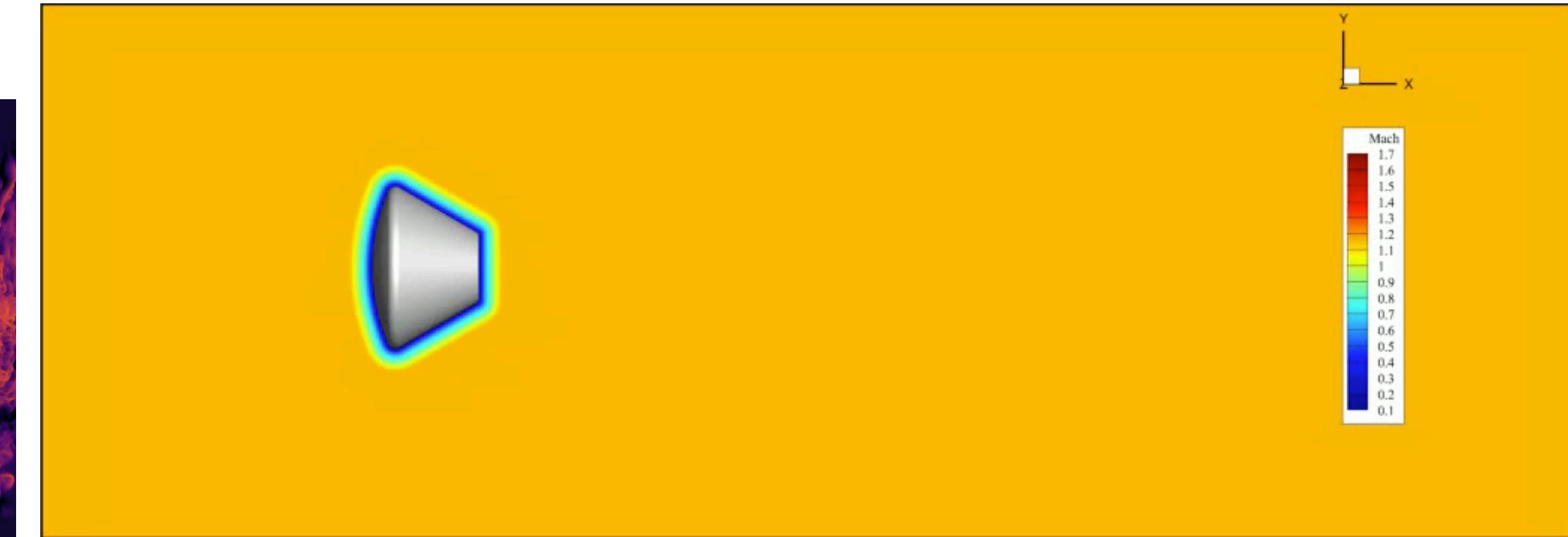


Kestrel



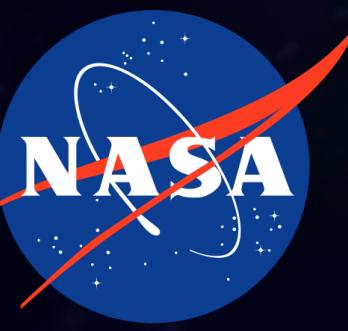
[6]

FUN3D

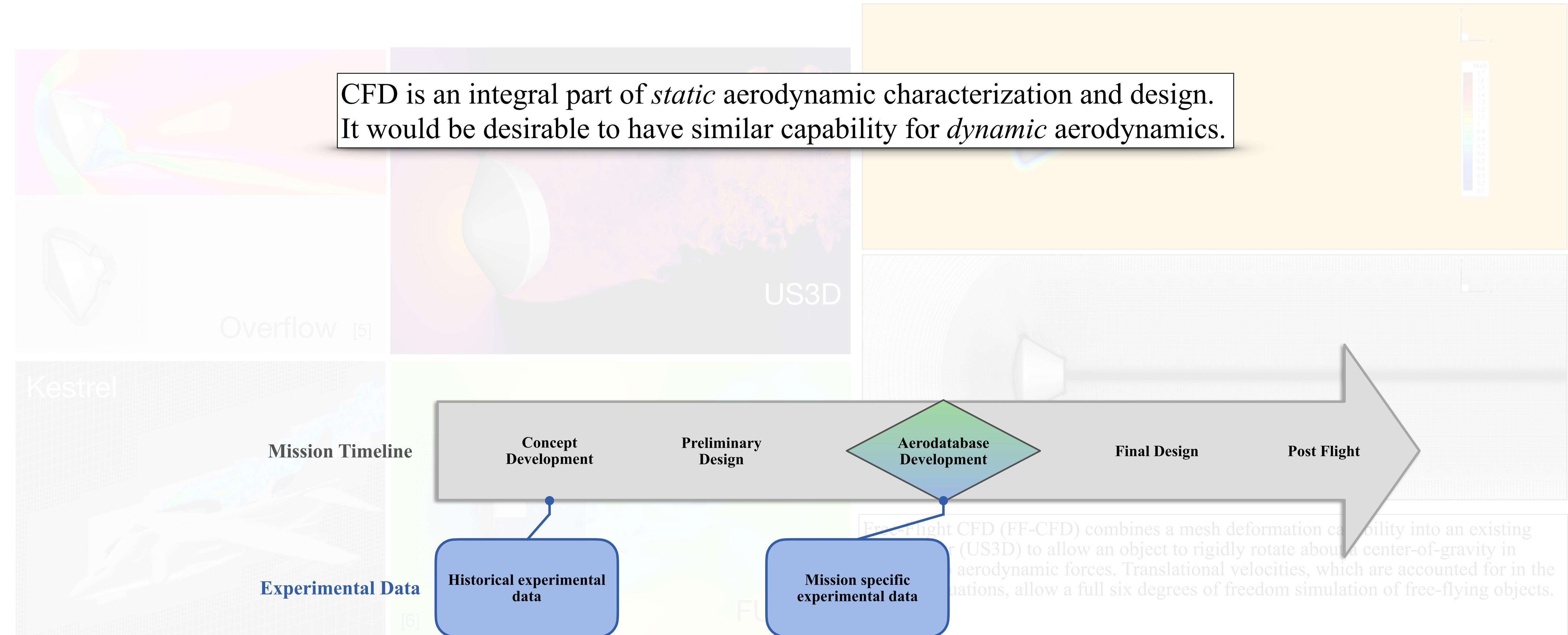


Free-Flight CFD (FF-CFD) combines a mesh deformation capability into an existing CFD solver (US3D) to allow an object to rigidly rotate about a center-of-gravity in response to aerodynamic forces. Translational velocities, which are accounted for in the discrete equations, allow a full six degrees of freedom simulation of free-flying objects.

# Computational Capabilities

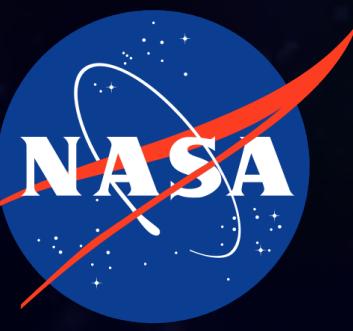


CFD is an integral part of *static* aerodynamic characterization and design. It would be desirable to have similar capability for *dynamic* aerodynamics.

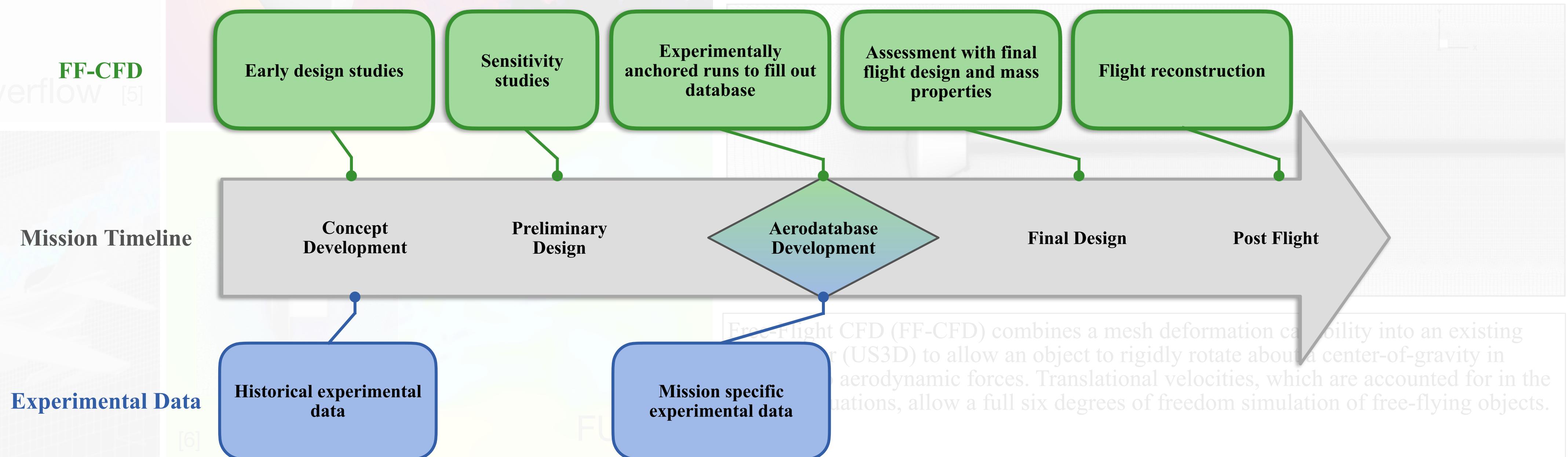


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# Computational Capabilities

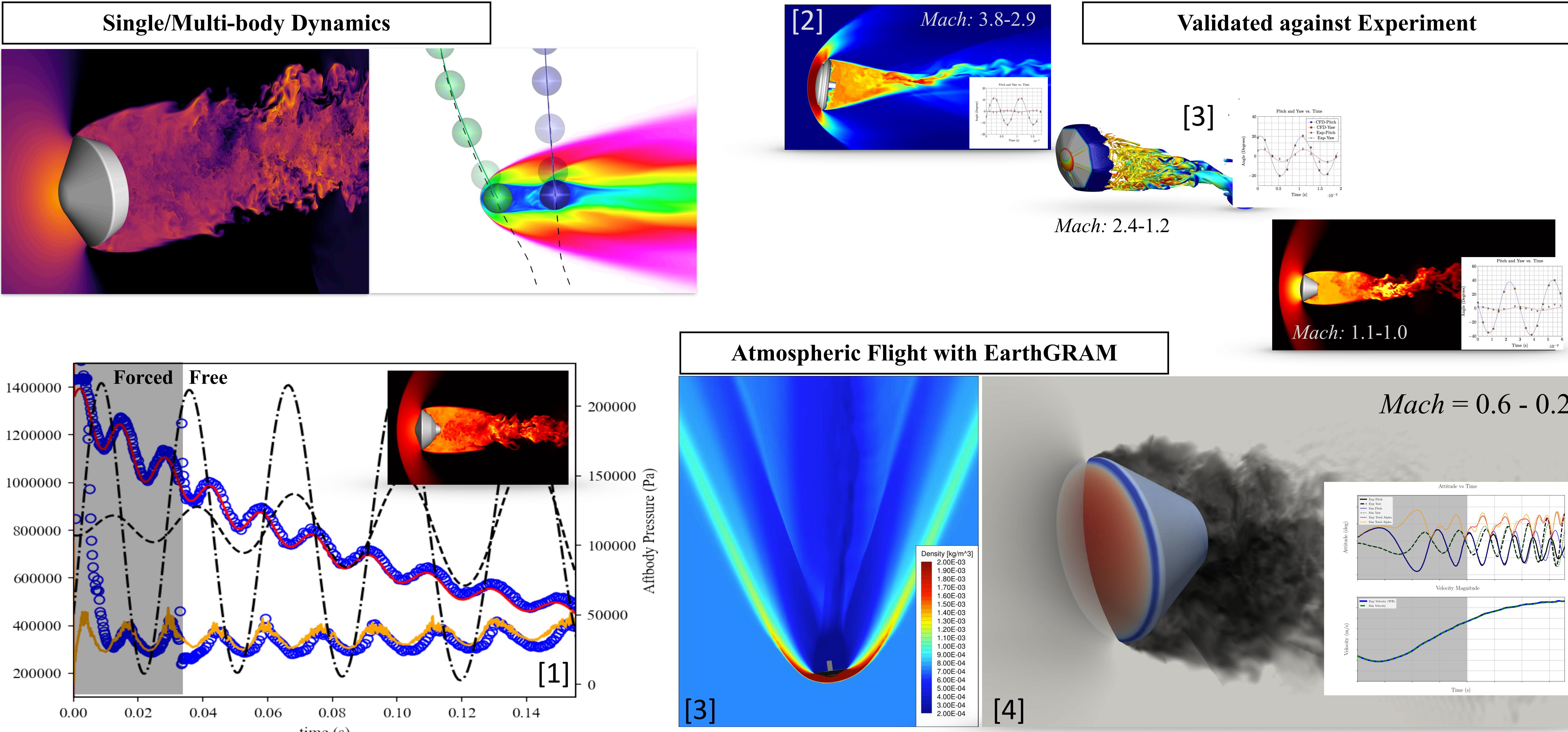


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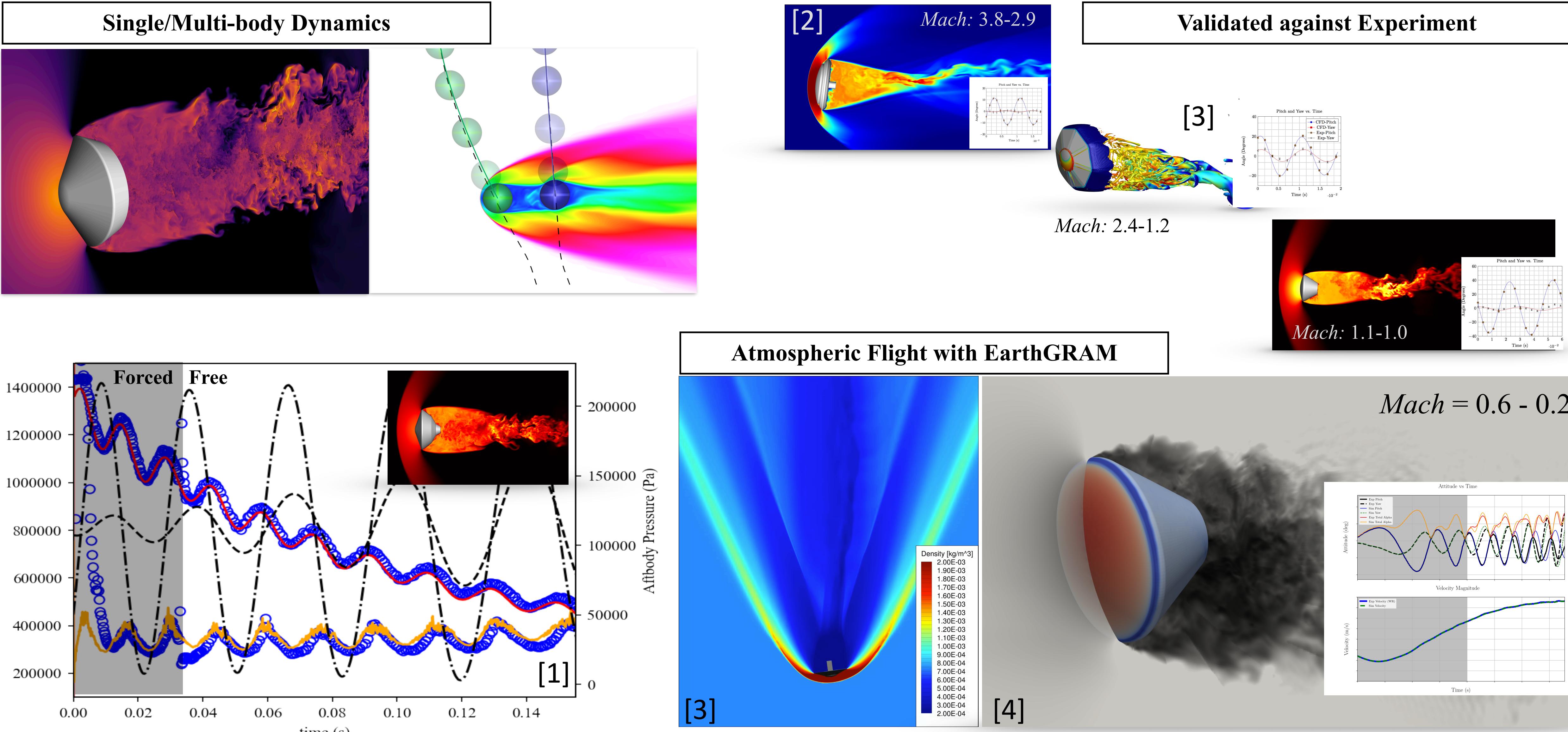


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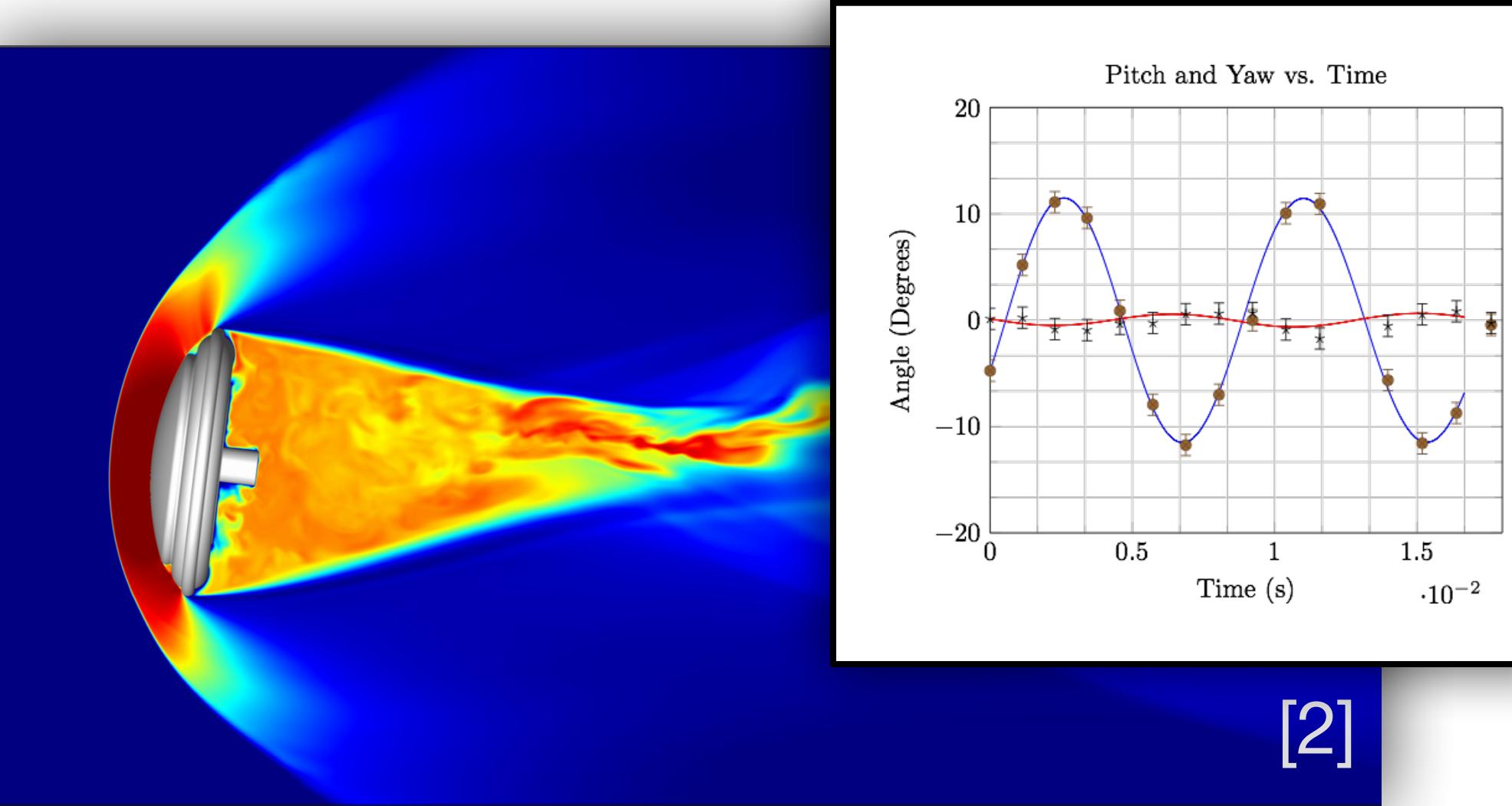
# Current State of the Art



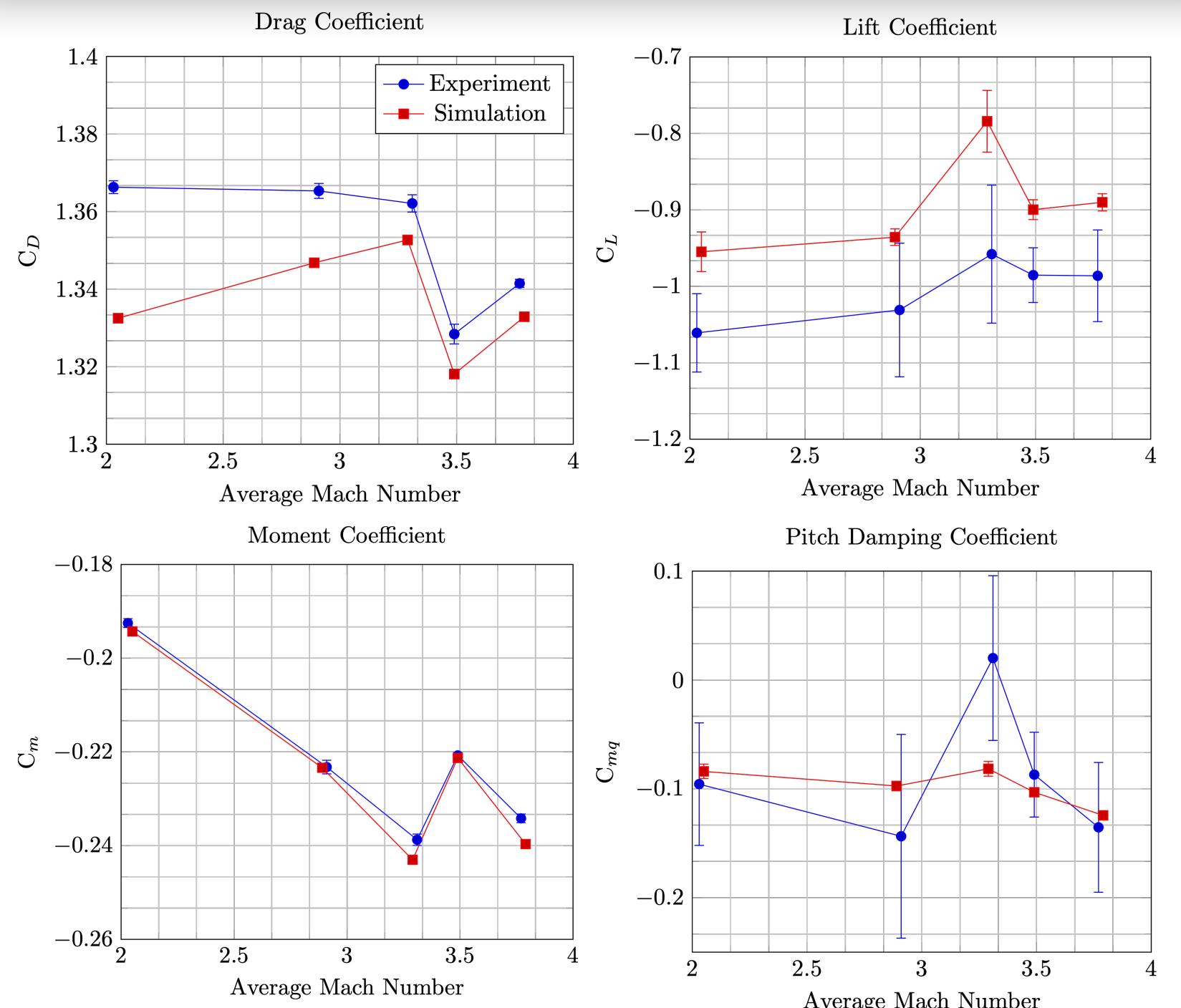
# Current State of the Art



# Free-Flight CFD Data as Input to Heritage Methods



[2]

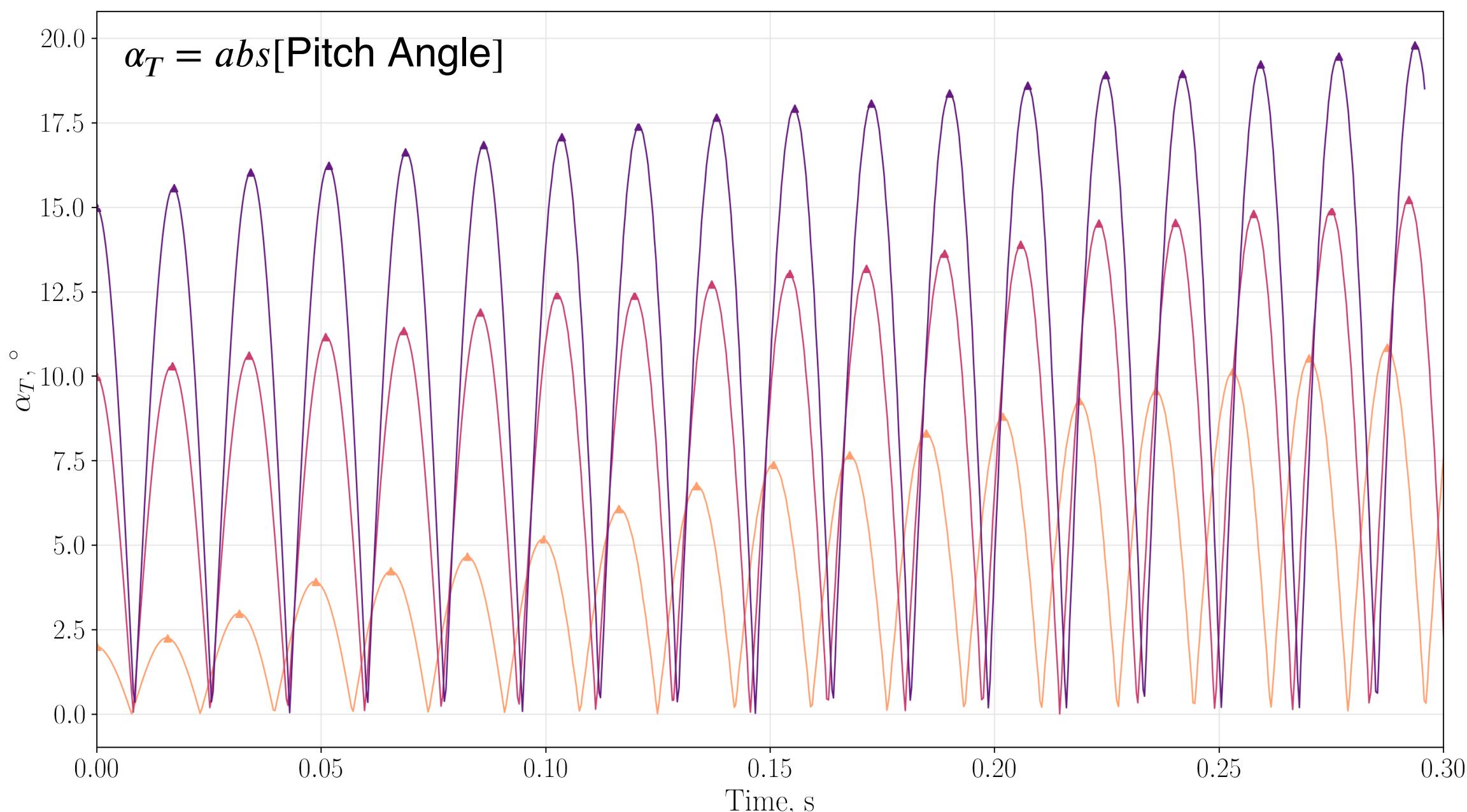
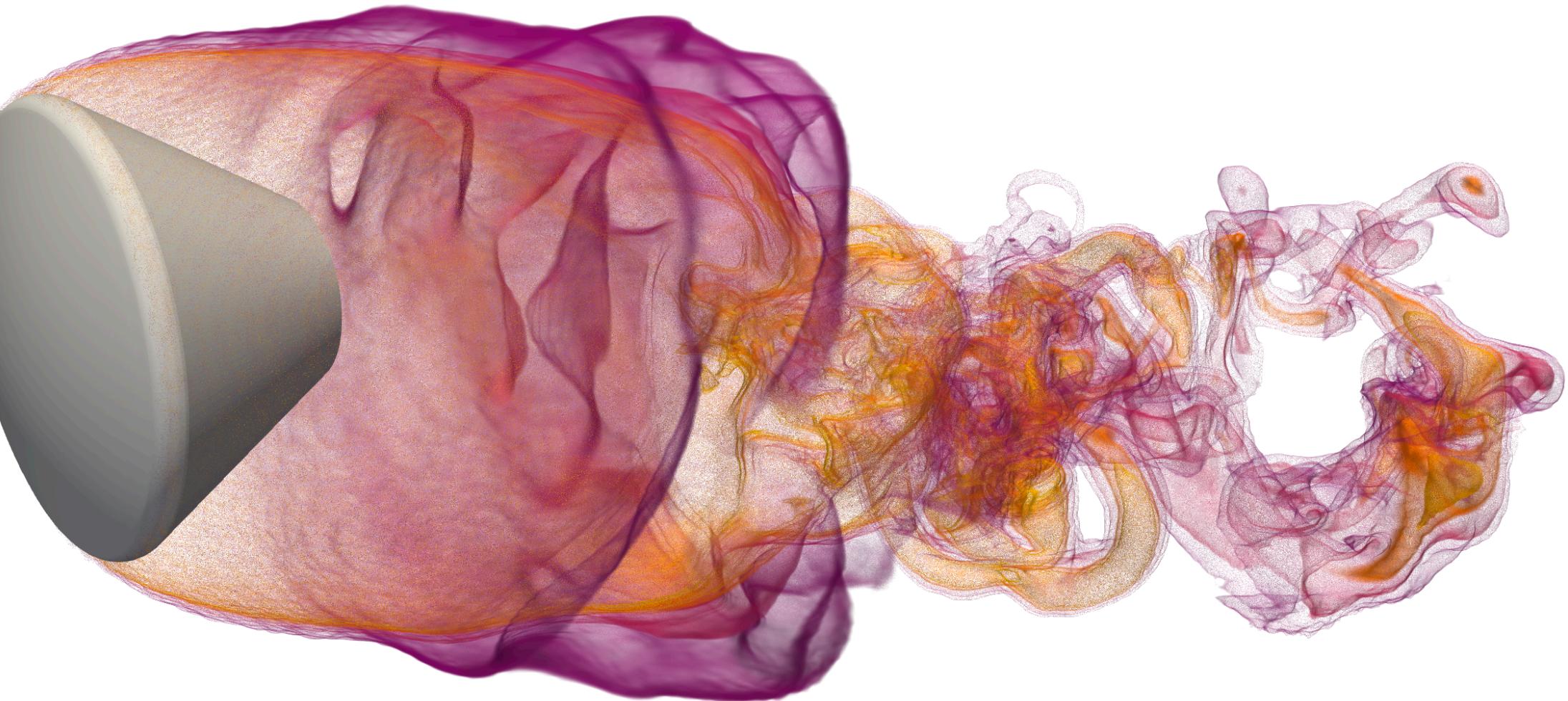


- Dynamic stability is often characterized by the pitch damping coefficient ( $C_{m_q}$ )
- Derivations of pitch damping coefficient in previous studies were obtained using the aerodynamic software CADRA
  - Results shows good comparison between simulation and ballistic range results
  - Required significant coarsening from order 100,000 time steps of CFD data down to 16 data points to obtain 1-to-1 comparison with BR data
- Rich datasets from FF-CFD simulations present an opportunity to apply new data reduction approaches

# Data Reduction for Free-Flight CFD



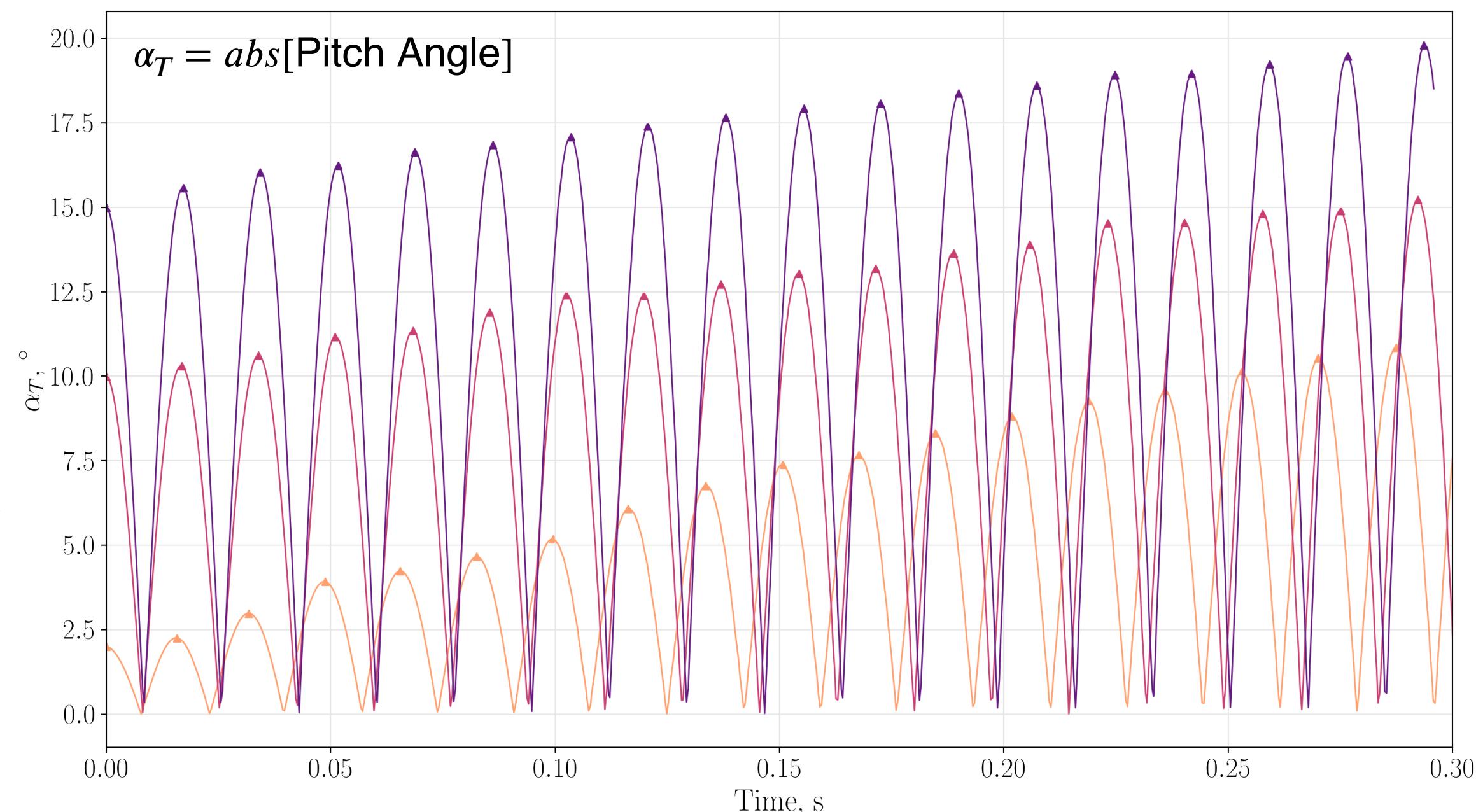
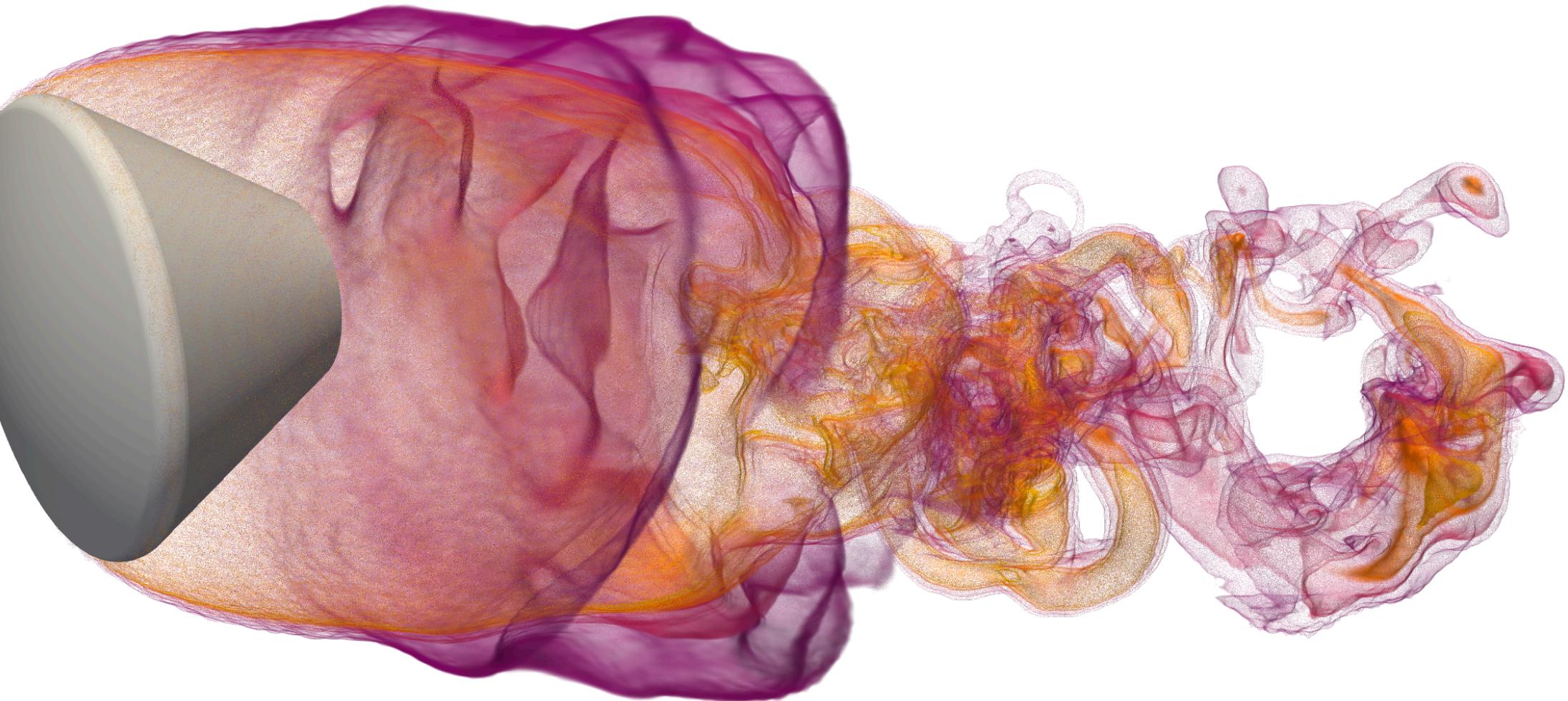
- PYnematics software suite to process FF-CFD output
  - A python suite of tools available to post-process FFCFD data and generate static and dynamic aero-coefficients
- Schoenenberger [5] states that (within assumptions of derived models) an equivalent  $C_{m_q}$  can be derived from 1- 2- or 3-DoF simulations
- Two methods developed for using FF-CFD 1-DoF analysis to computing dynamic coefficients
  1. Run reduced 1DoF FF-CFD simulations and then:
  - 2a. Use analytical forms of equations to generate non-linear fits to  $C_{m_q}$  as a function of oscillation amplitude
  - 2b. Use inverse estimation and 1-DoF EOMs to identify optimal  $C_{m_q}$  curve as a function of instantaneous angle of attack.



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# Use of Analytical Solutions To Compute Pitch Damping

- Methodology for using FF-CFD 1-DoF analysis to compute dynamic coefficients [6]

**1-DoF Analytical Solution**

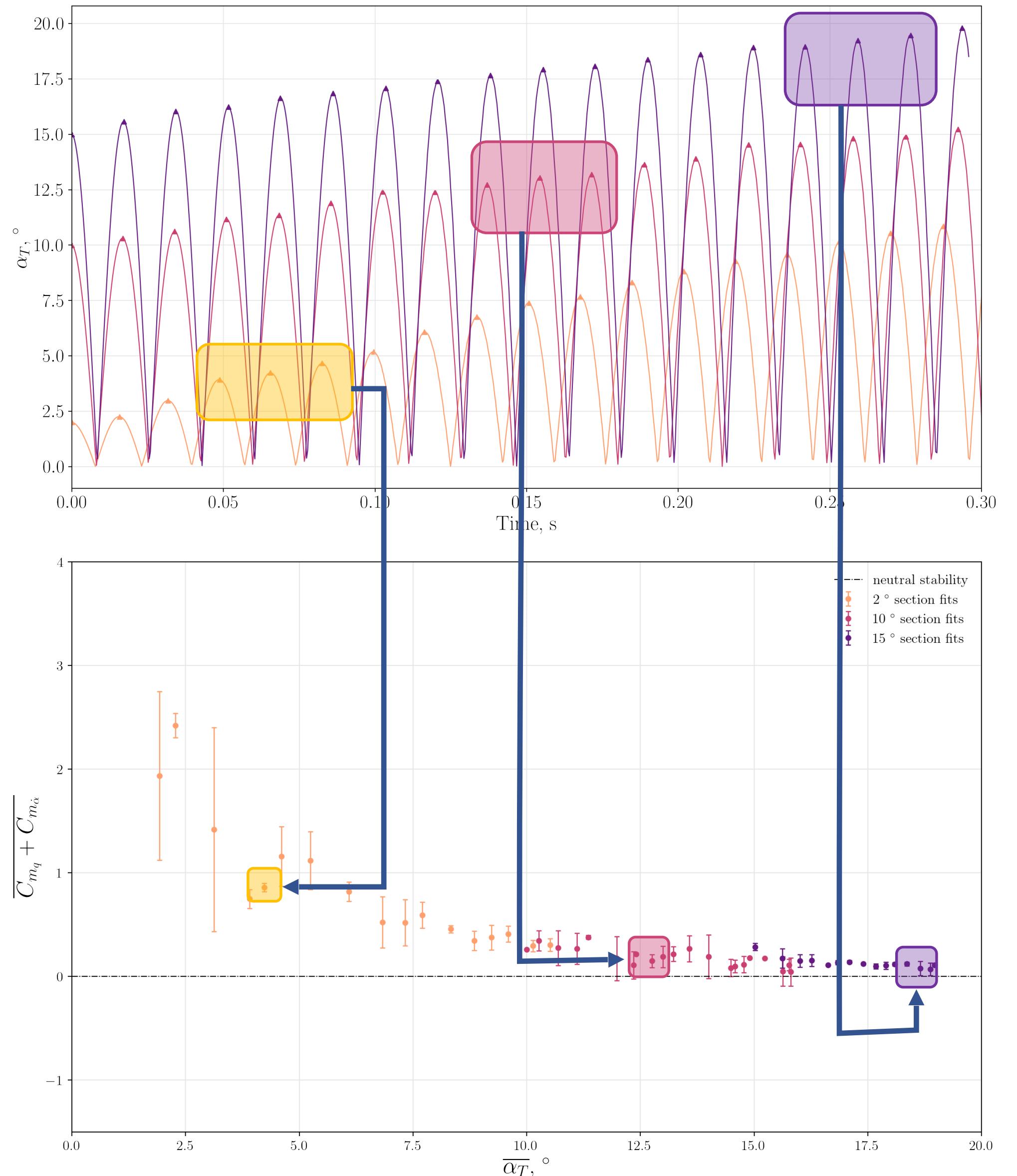
$$\ddot{\alpha} - \frac{\rho V_\infty S d^2}{4I} (C_{m_q} + C_{m_{\dot{\alpha}}}) \dot{\alpha} - \frac{\rho V_\infty^2 S d}{2I} C_{m_{\alpha}} \alpha = 0$$

$$\alpha = A e^{\xi_1 t} \cos(\omega t + \delta) \quad \longrightarrow \quad \xi_1 = \frac{\rho V S d^2}{8I} (C_{m_q} + C_{m_{\dot{\alpha}}})$$

- Algorithm:

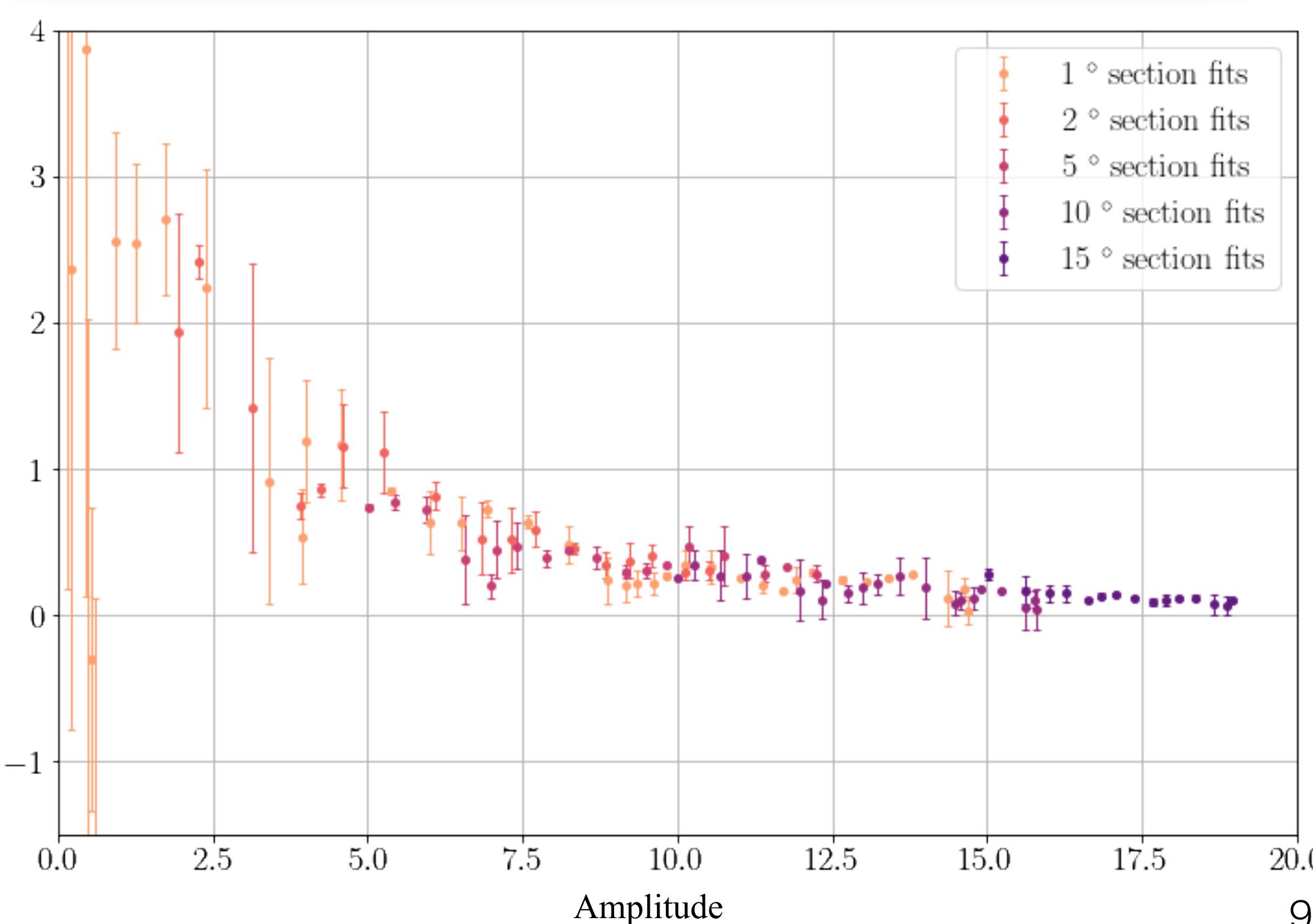
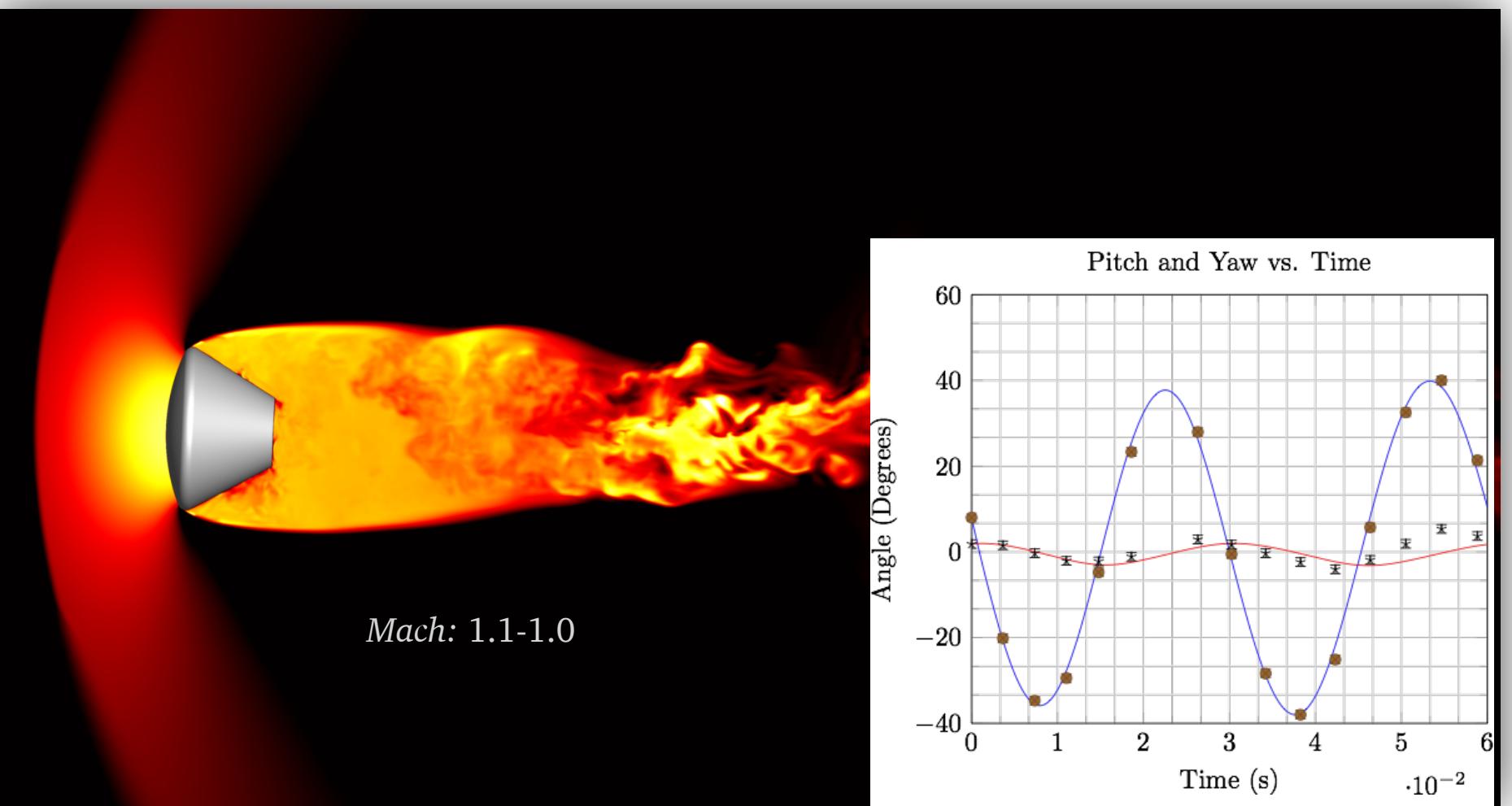
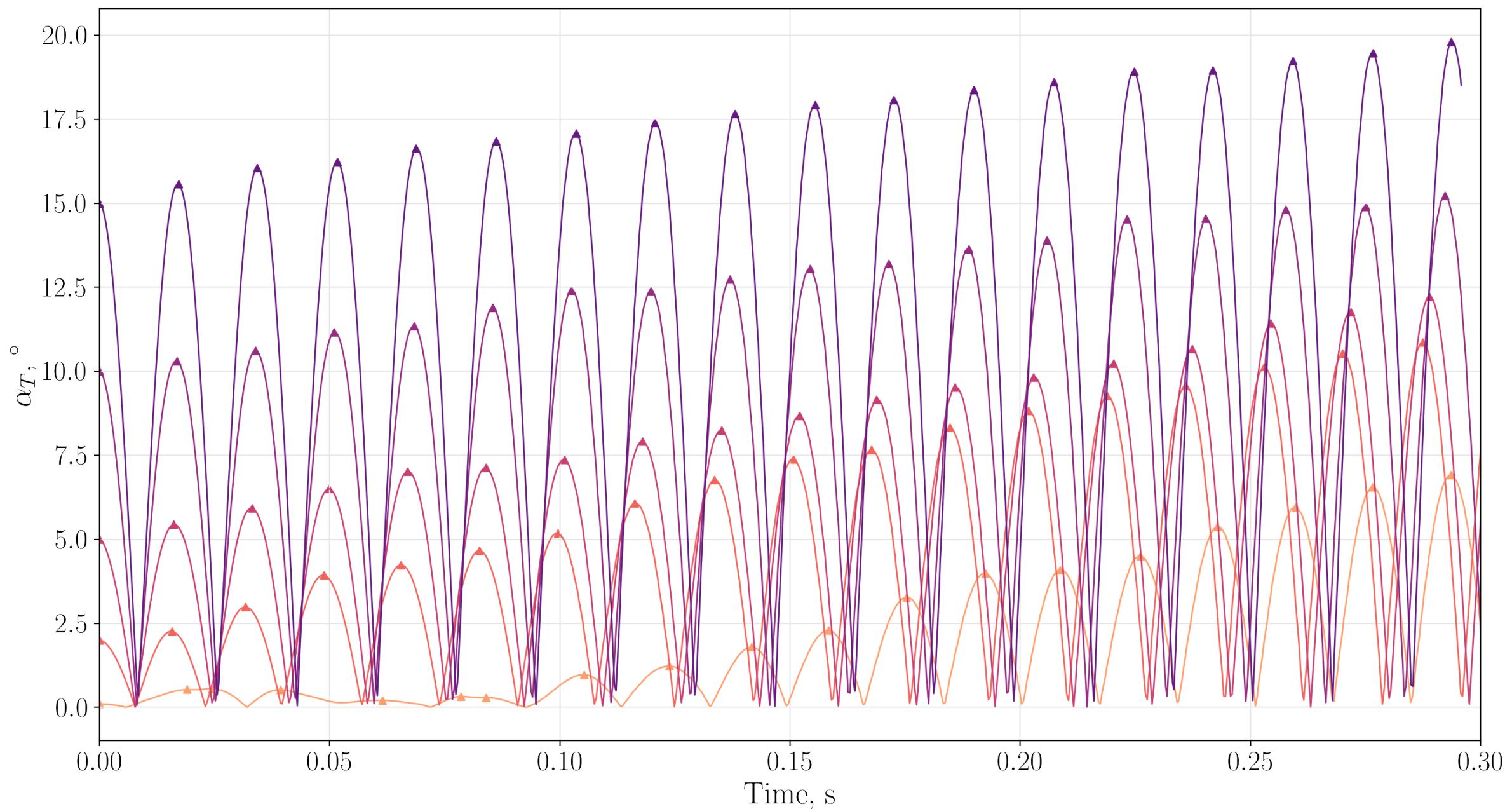
- For each  $\alpha_0$ :
  - Using a stencil of 3-5 peaks, fit analytical expression for  $\bar{C}_{m_q}$  to segments of the trajectory to capture local amplitude growth (or decay)
  - Add this  $\bar{C}_{m_q}$  value to our larger  $\bar{C}_{m_q}$  vs a space at the average total angle of attack for the peaks within that stencil
  - Move to next set of stenciled peaks and repeat
- Combine all individual stencil fits into amplitude bins
- Curve fit bins to get  $\bar{C}_{m_q}$  as a function of amplitude

Results in a mapping across all *amplitudes*



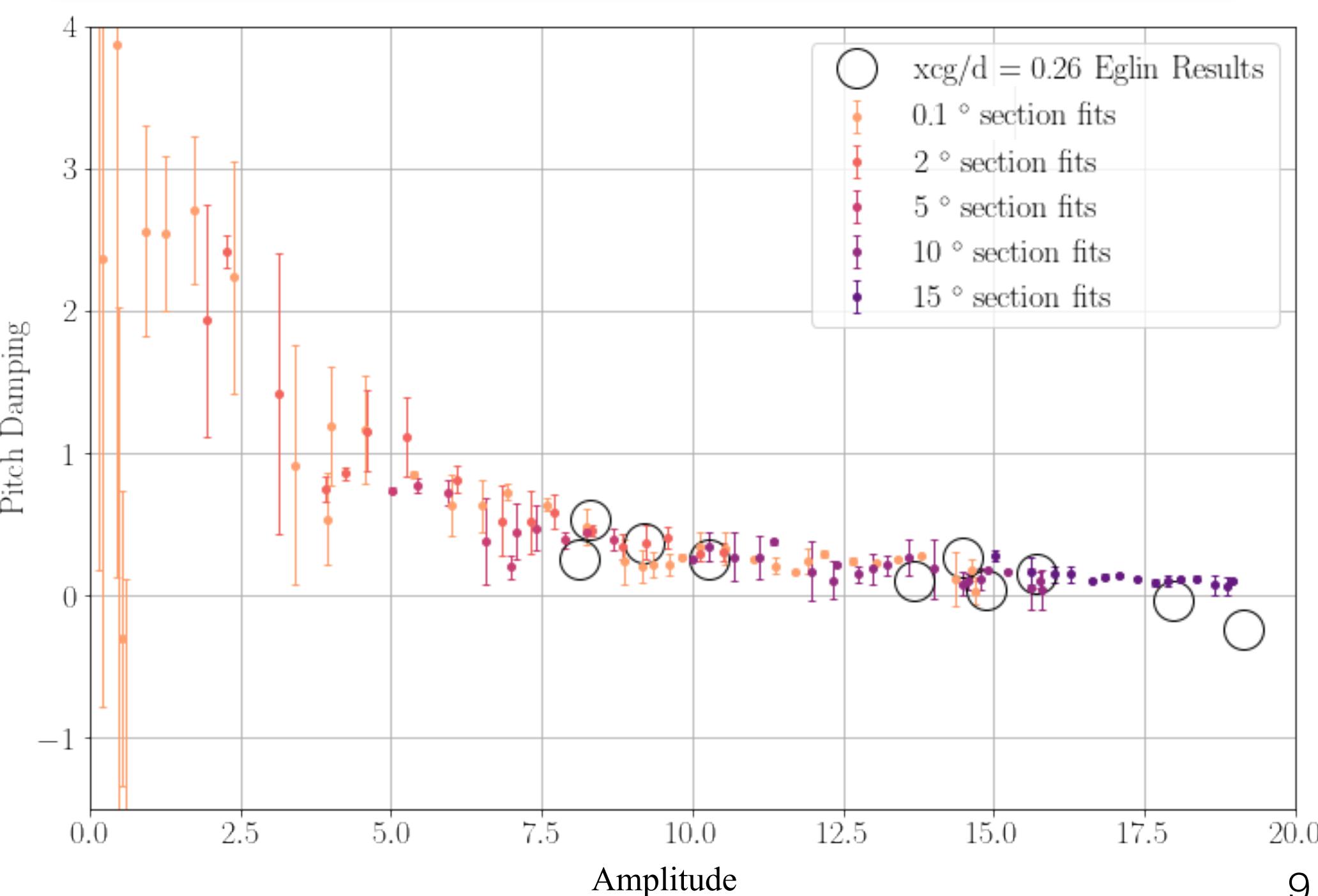
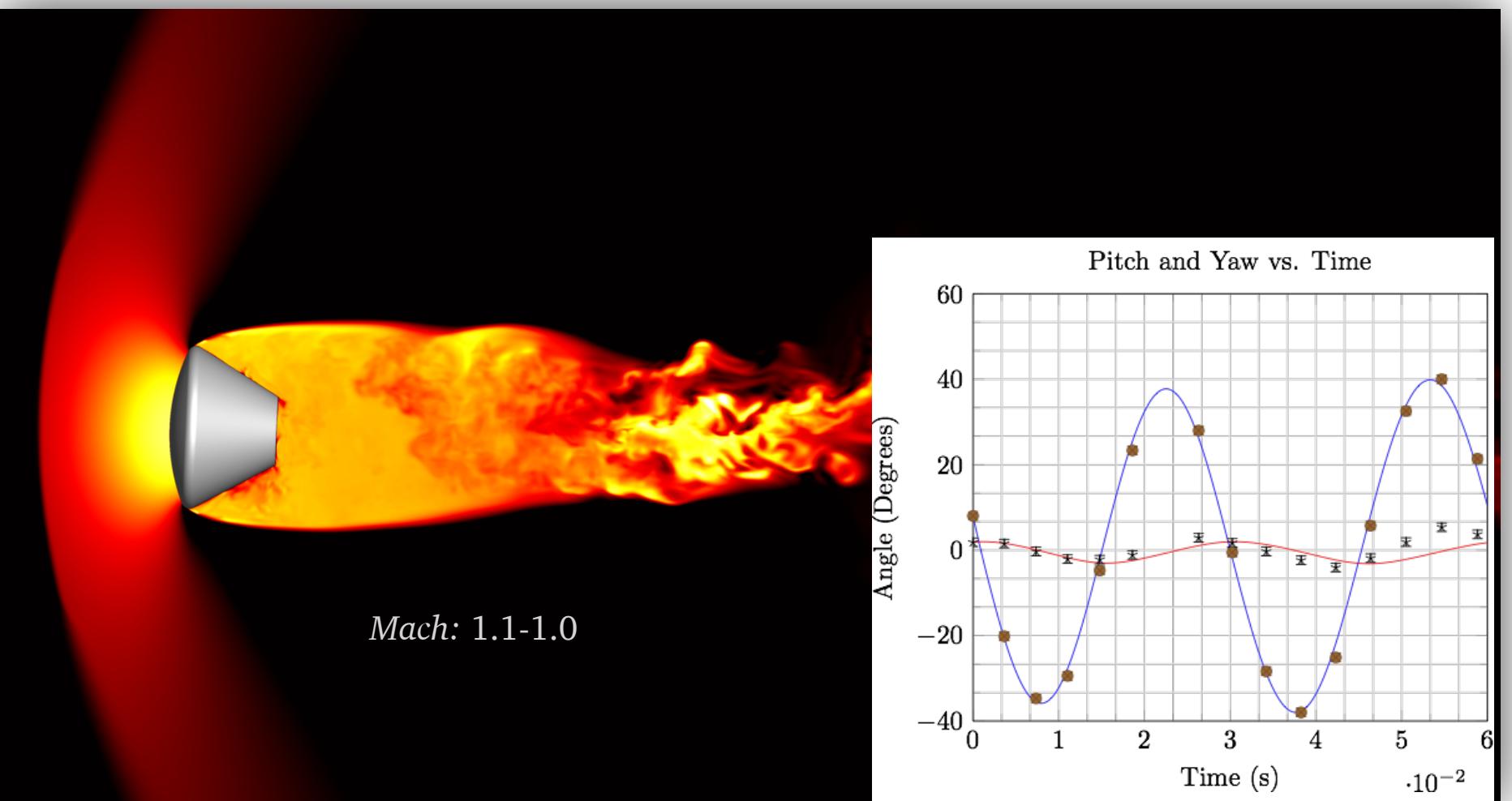
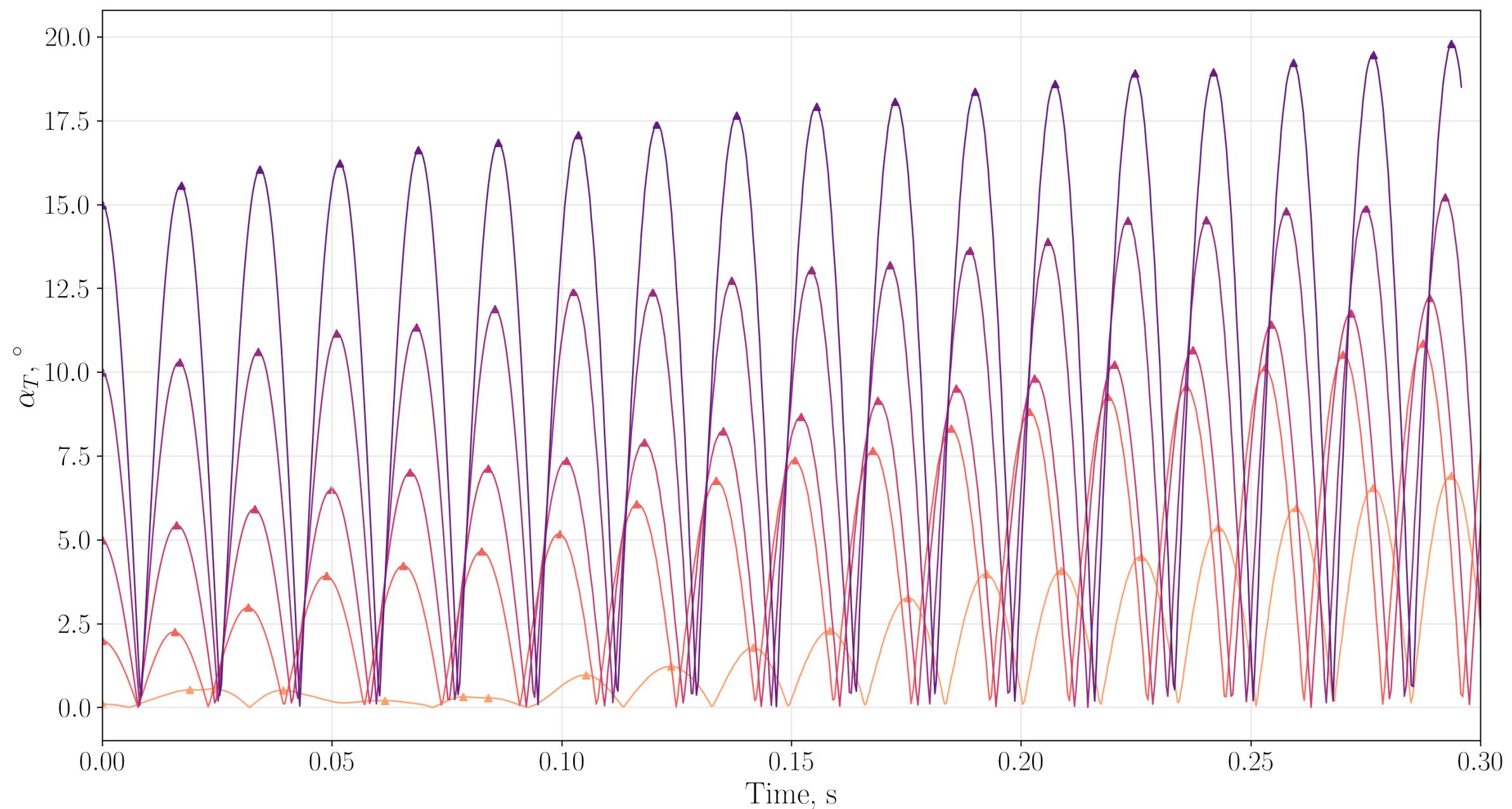
# Comparison to Crew Module

- 1-DoF FF-CFD dynamic analysis applied to Orion CM
  - Constant Mach=1.07 corresponding to mid Mach condition of HFFAF BR Shot 2366
- All initial amplitudes grow with no observable stable limit cycle
- Comparison of derived distribution of  $C_{m_q}$  section fits from 1-DoF trajectories agree well with experimental data obtained at a separate facility
  - Results suggest dynamic behavior is consistent between facility and simulation
- Static coefficients can be obtained from collection 1-DoF trajectories



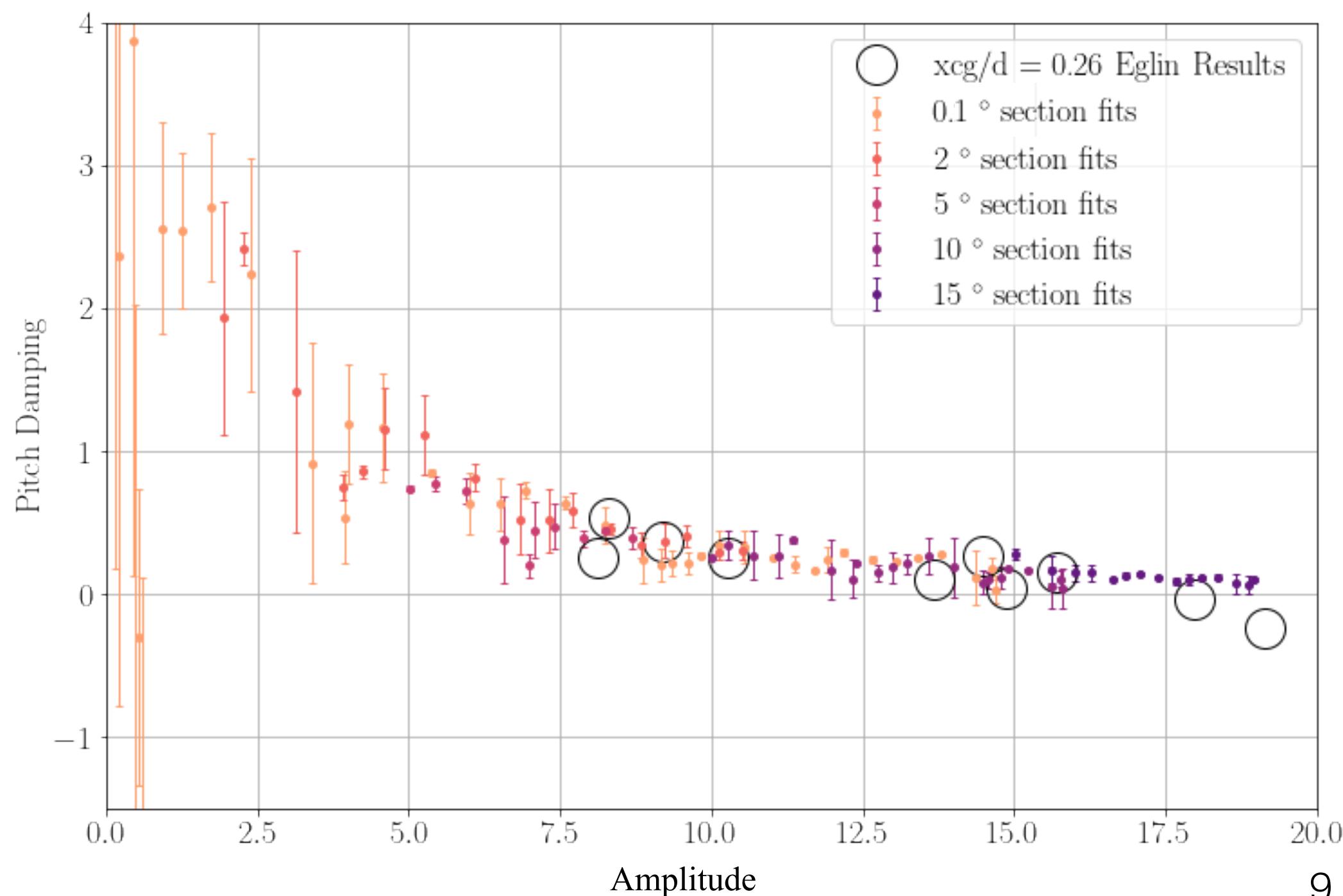
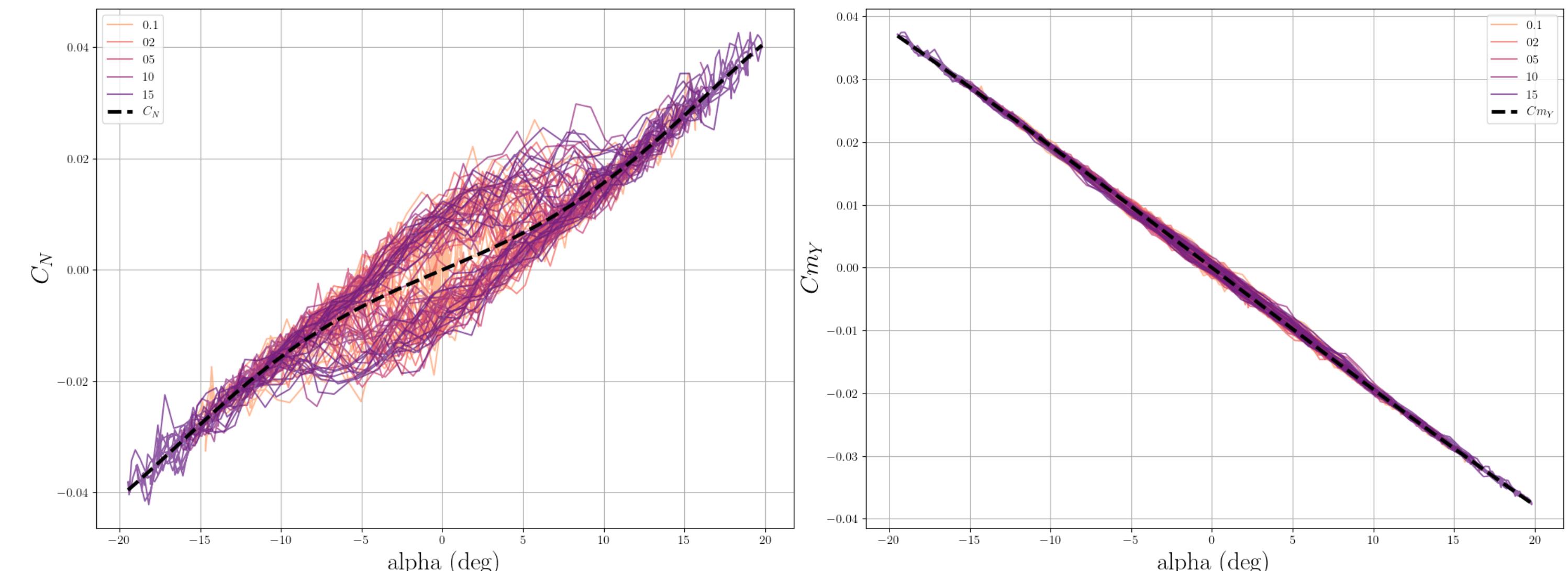
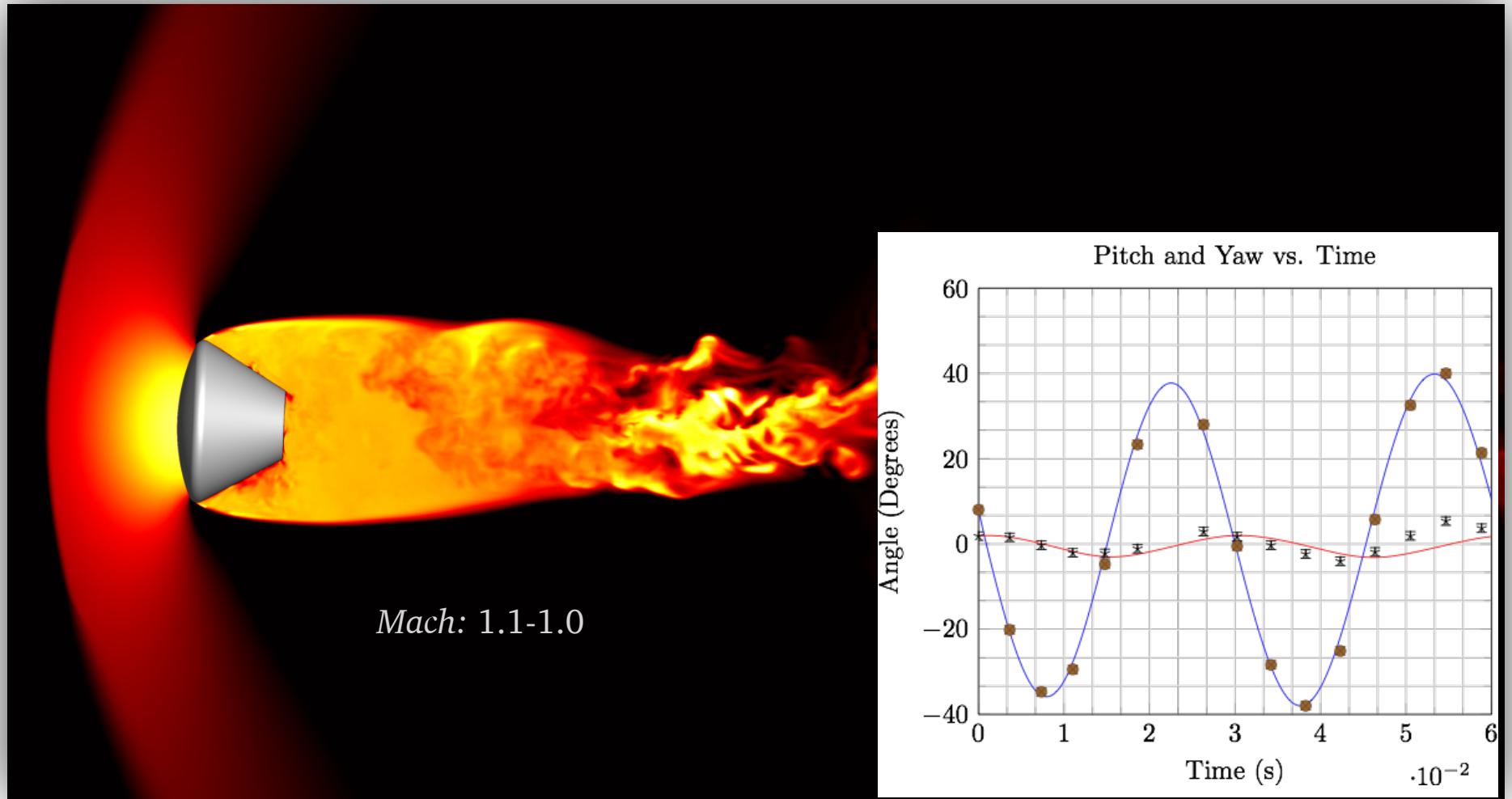
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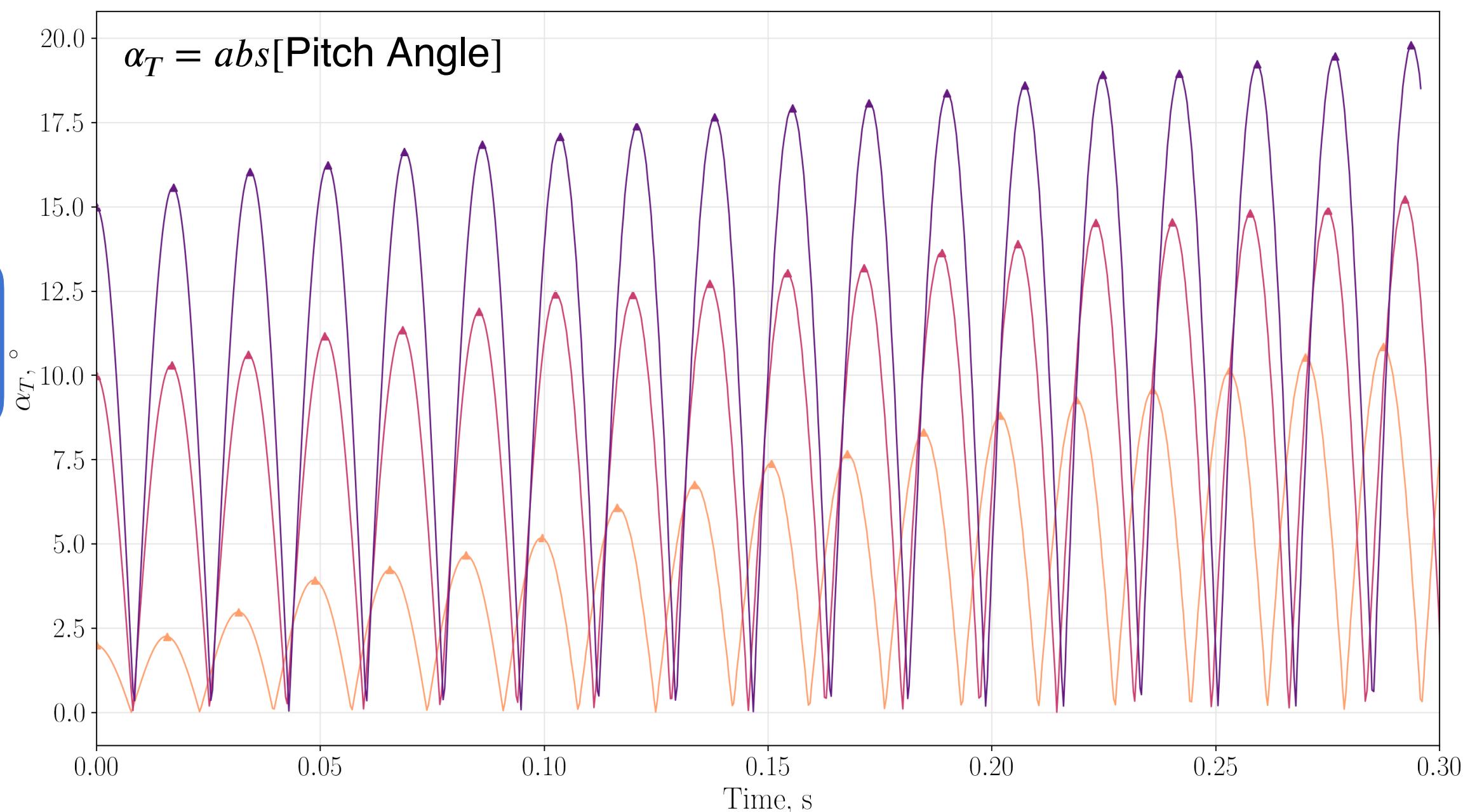
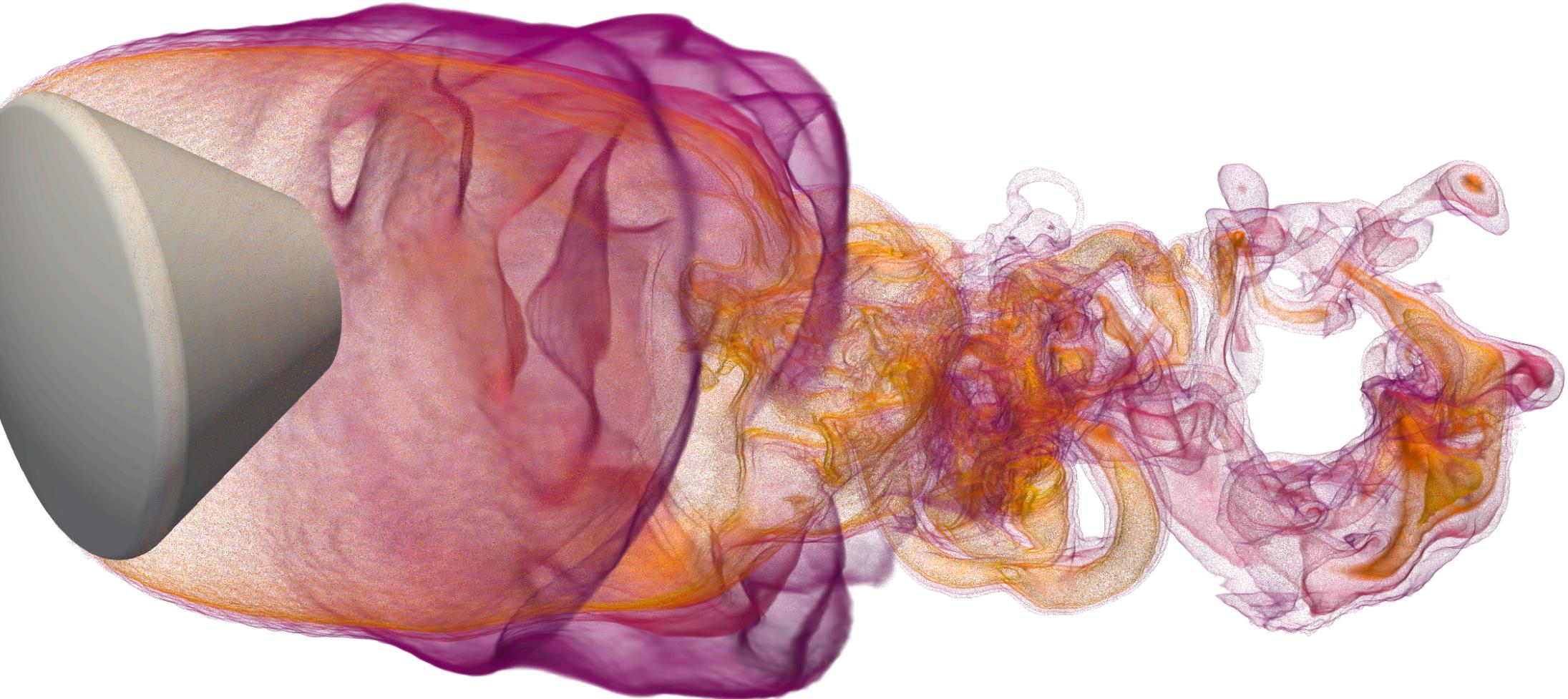
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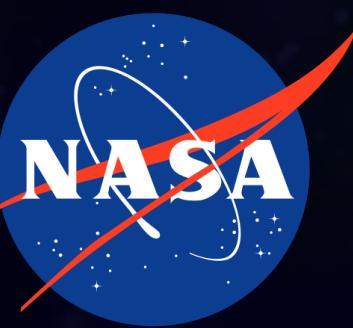
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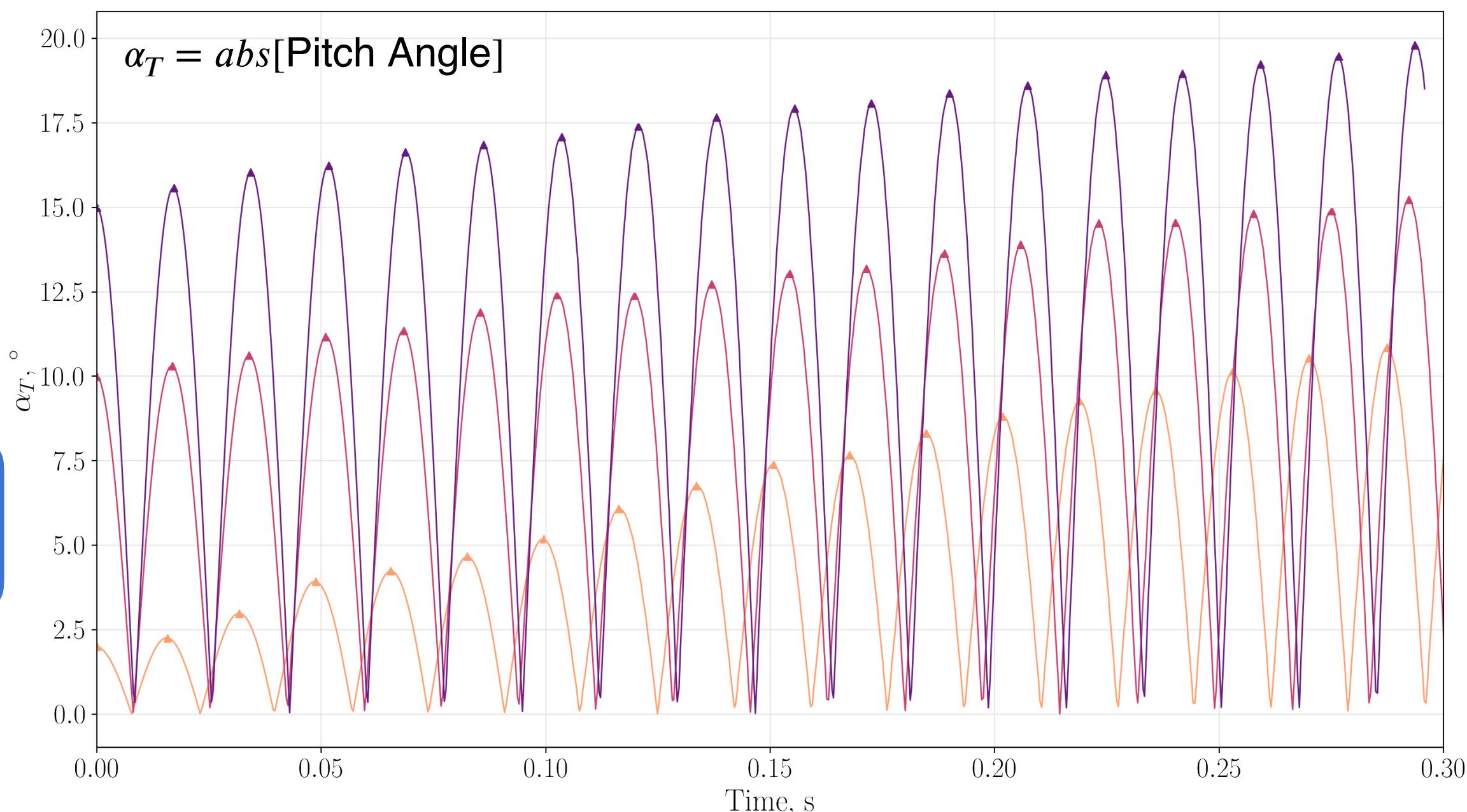
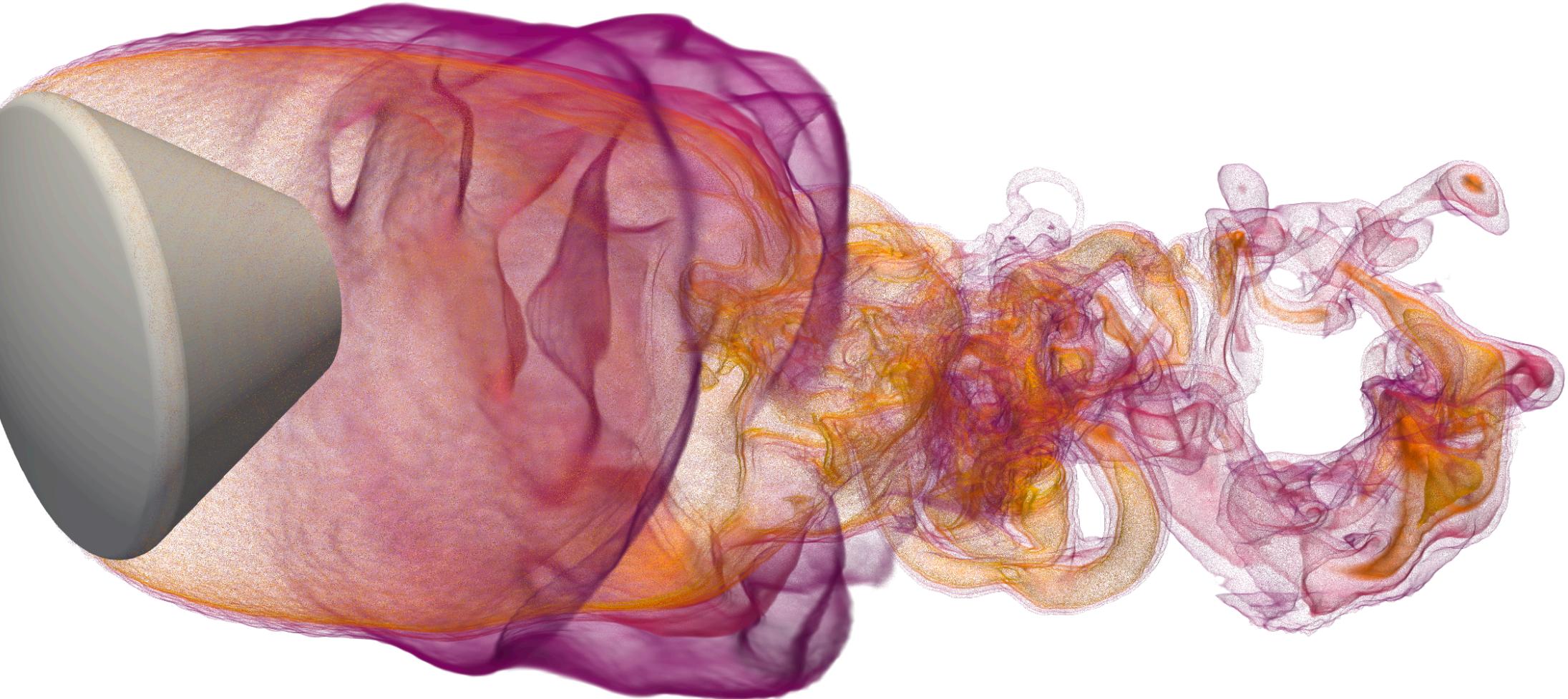
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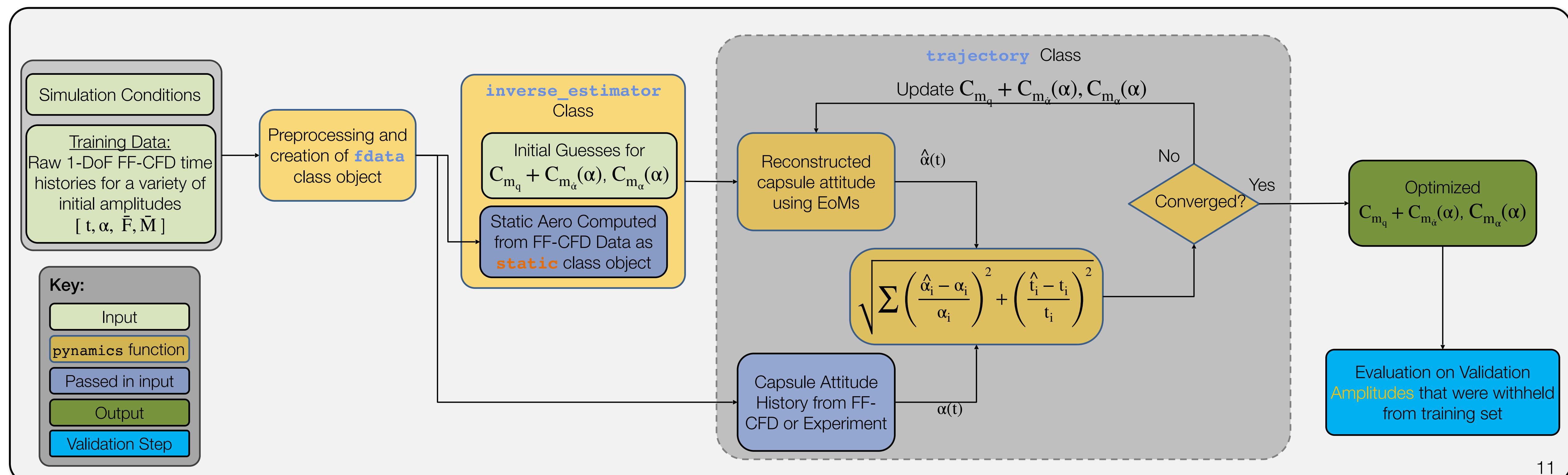
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# Inverse Estimation of Pitch Damping at Constant Mach (1-DoF)

End-to-End pipeline has been created for extracting static and dynamic aero coefficients from 1-DoF (free-to-pitch) FF-CFD simulations

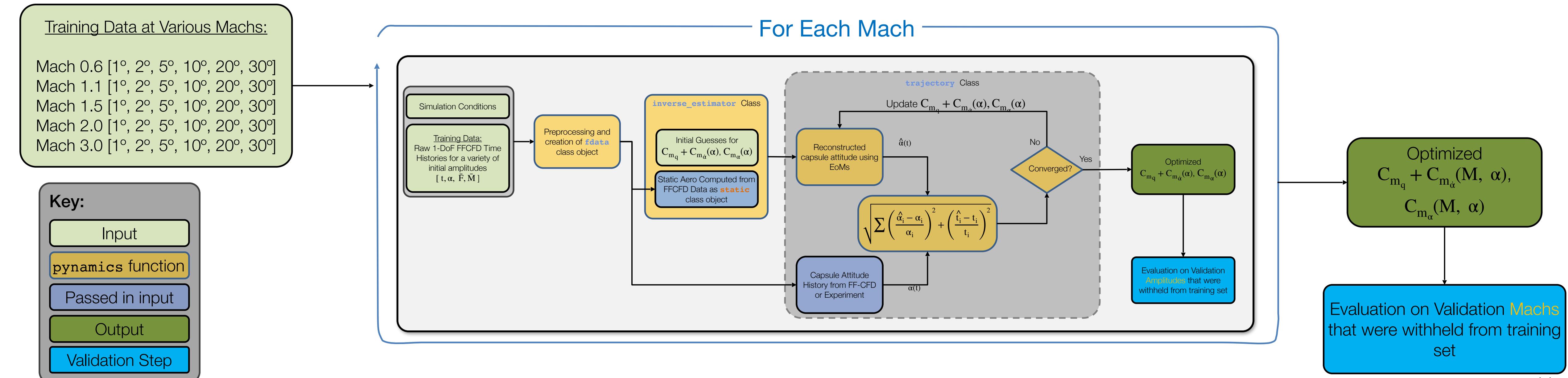
- Theory suggests and previous work has shown that pitch damping coefficient derived from 1-DoF is equivalent to that from higher DoF simulations
- Reconstruction: Using the ODE derived by Schoenenberger, Queen: 
$$\ddot{\alpha} - \frac{\rho VS}{2m} \left( -C_{L_\alpha} + \frac{md^2}{2I} (C_{m_q} + C_{m_{\dot{\alpha}}}) \right) \dot{\alpha} - \frac{\rho V^2 S d}{2I} C_{m_\alpha} \alpha = 0$$
 integrate forwards in time using Python's **solve\_ivp** to generate a trajectory history
  - Requires: dof simplifications, geometric constants, static aero coefficients,  $\alpha_0$  (initial amplitude),  $\dot{\alpha}_0$  (local maxima), and  $C_{m_q} + C_{m_{\dot{\alpha}}}$  as a function of  $\alpha$
- Optimization: Send Python's **scipy.optimize.minimize** a functional form of the pitch damping curve with an initial guess, wrap the reconstruction (**solve\_ivp**) scheme in the optimizer, and iterate on input curve coefficients to minimize the normalized  $L_2$  residual between peak amplitudes
  - Optional inclusion of peak times in the objective function allows for co-optimization of  $C_{m_\alpha}$  (shown below). Otherwise, compute in static aero routine.



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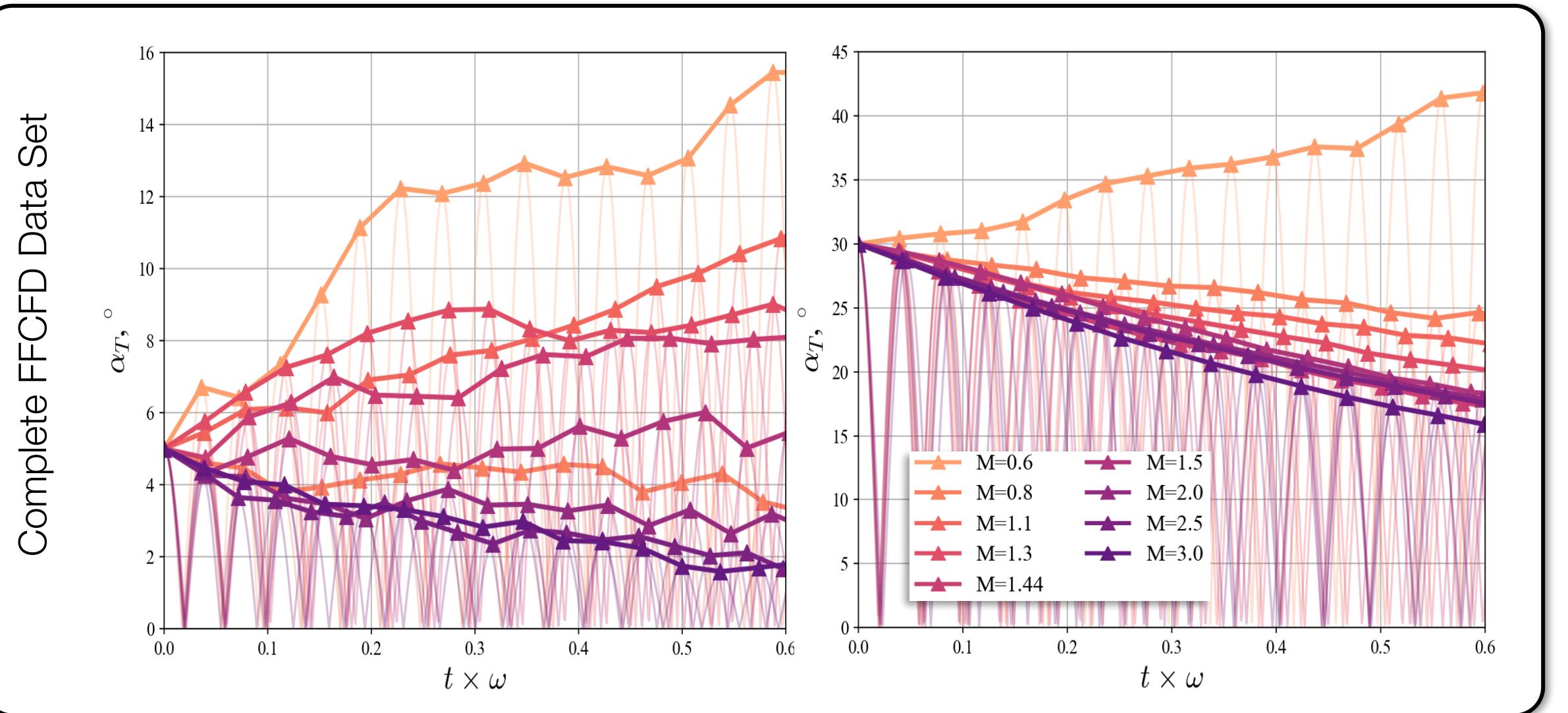
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$$\ddot{\alpha} - \frac{\rho VS}{2m} \left( -C_{L_\alpha} + \frac{md^2}{2I} (C_{m_q} + C_{m_{\dot{\alpha}}}) \right) \dot{\alpha} - \frac{\rho V^2 S d}{2I} C_{m_\alpha} \alpha = 0$$
 integrate forwards in time using Python's **solve\_ivp** to generate a trajectory history
  - Requires: dof simplifications, geometric constants, static aero coefficients,  $\alpha_0$  (initial amplitude),  $\dot{\alpha}_0$  (local maxima), and  $C_{m_q} + C_{m_{\dot{\alpha}}}$  as a function of  $\alpha$
- Optimization: Send Python's **scipy.optimize.minimize** a functional form of the pitch damping curve with an initial guess, wrap the reconstruction (**solve\_ivp**) scheme in the optimizer, and iterate on input curve coefficients to minimize the normalized  $L_2$  residual between peak amplitudes
  - Optional inclusion of peak times in the objective function allows for co-optimization of  $C_{m_\alpha}$  (shown below). Otherwise, compute in static aero routine.



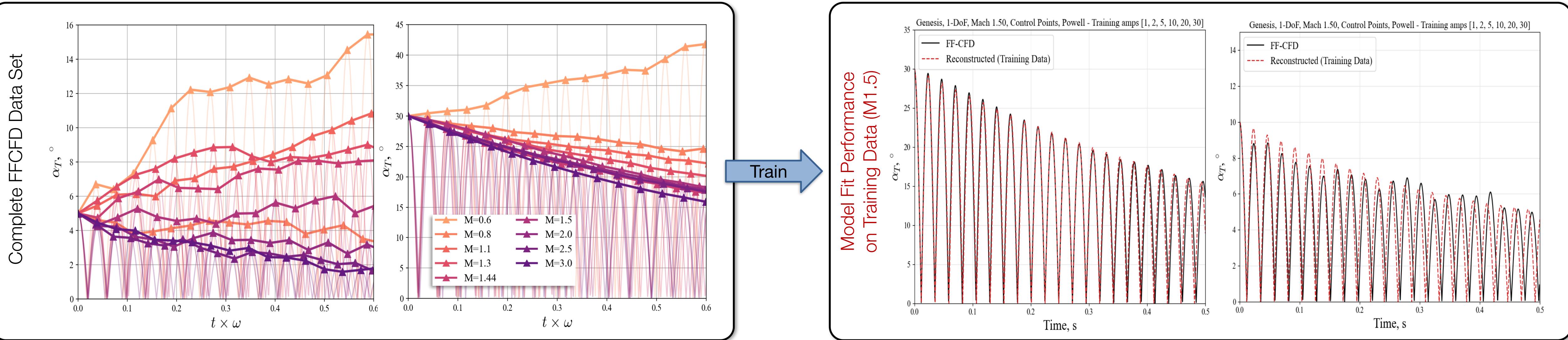
# End-to-End Example



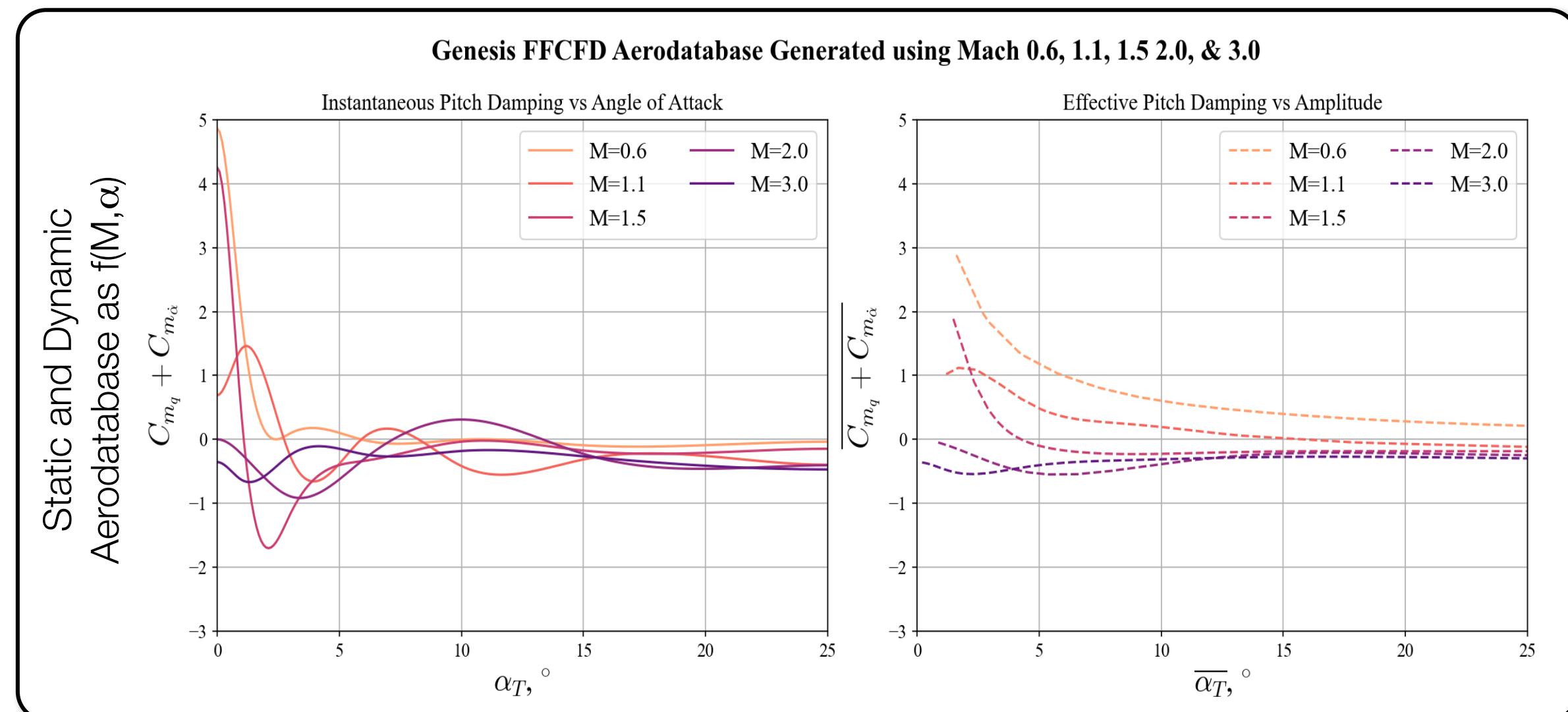
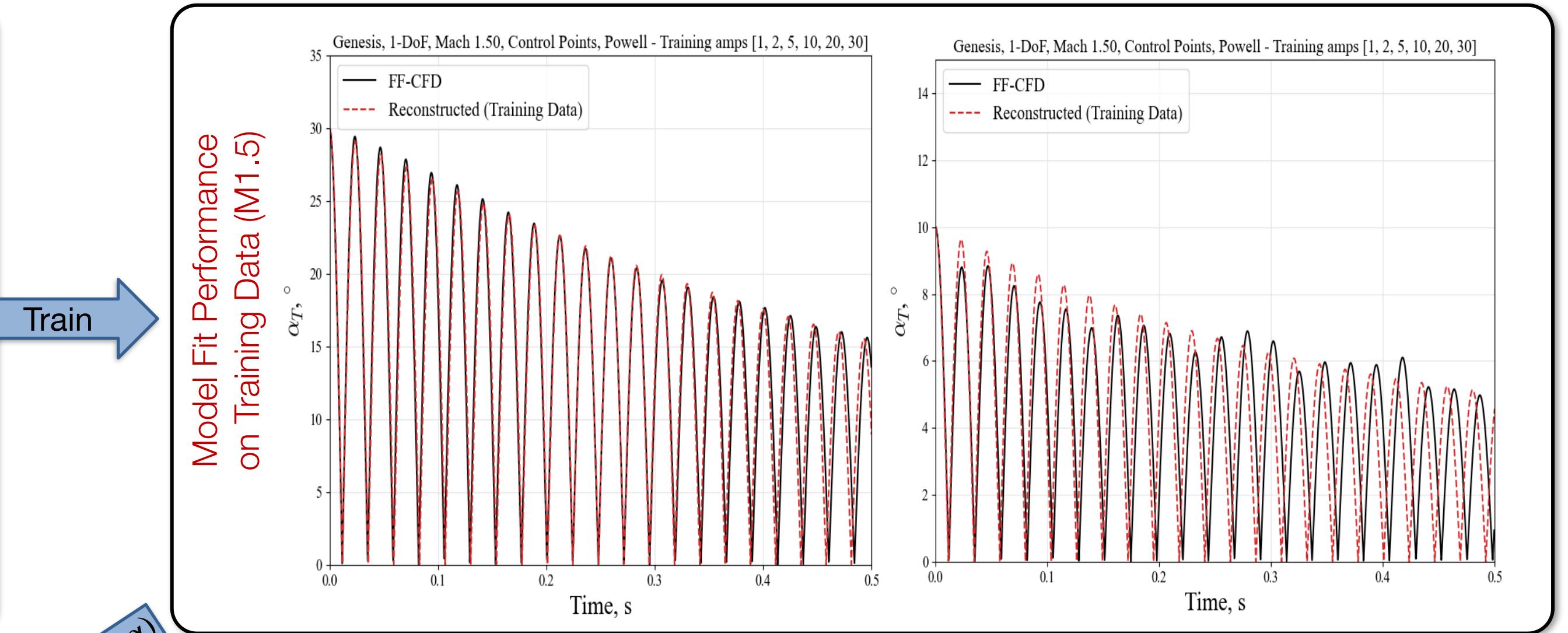
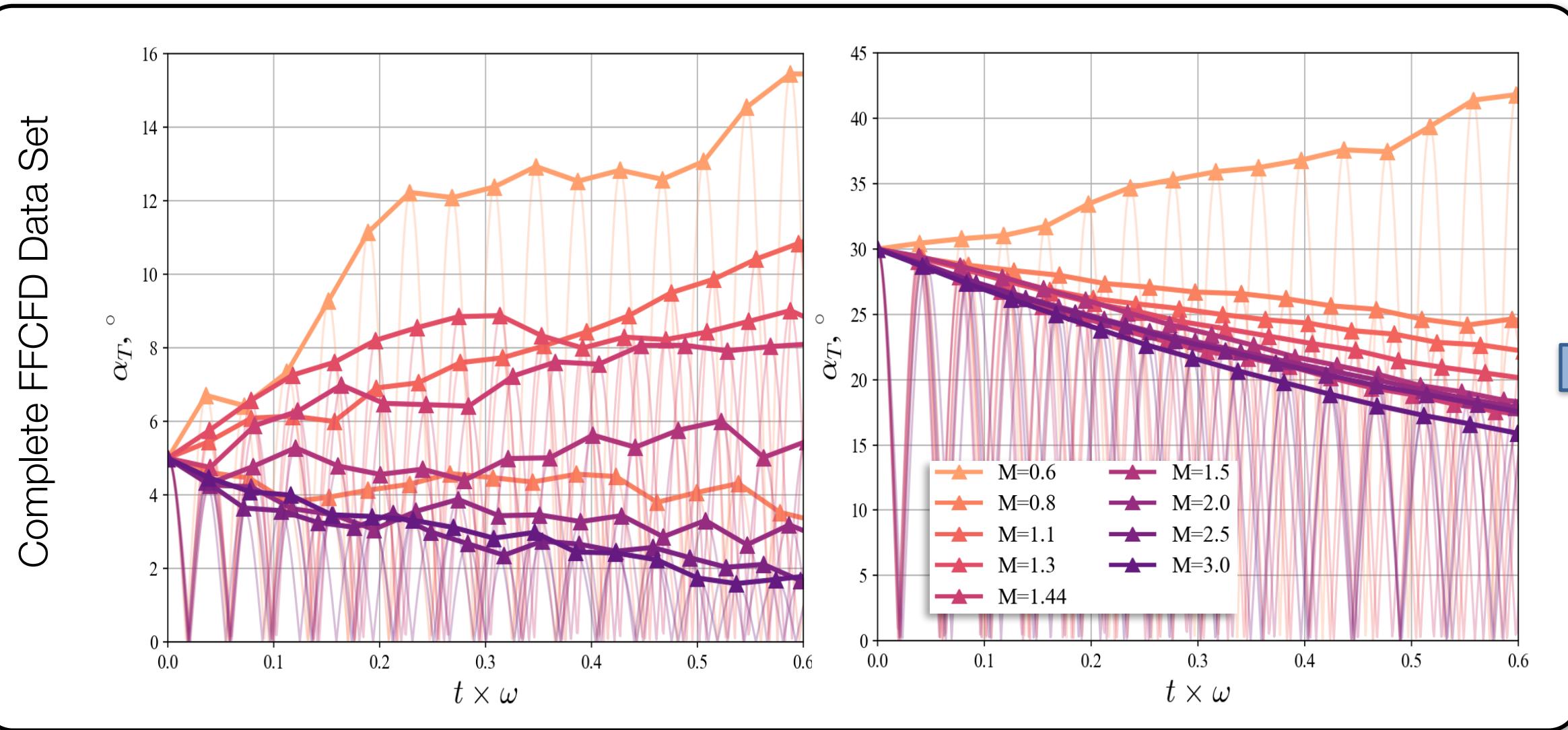
# End-to-End Example



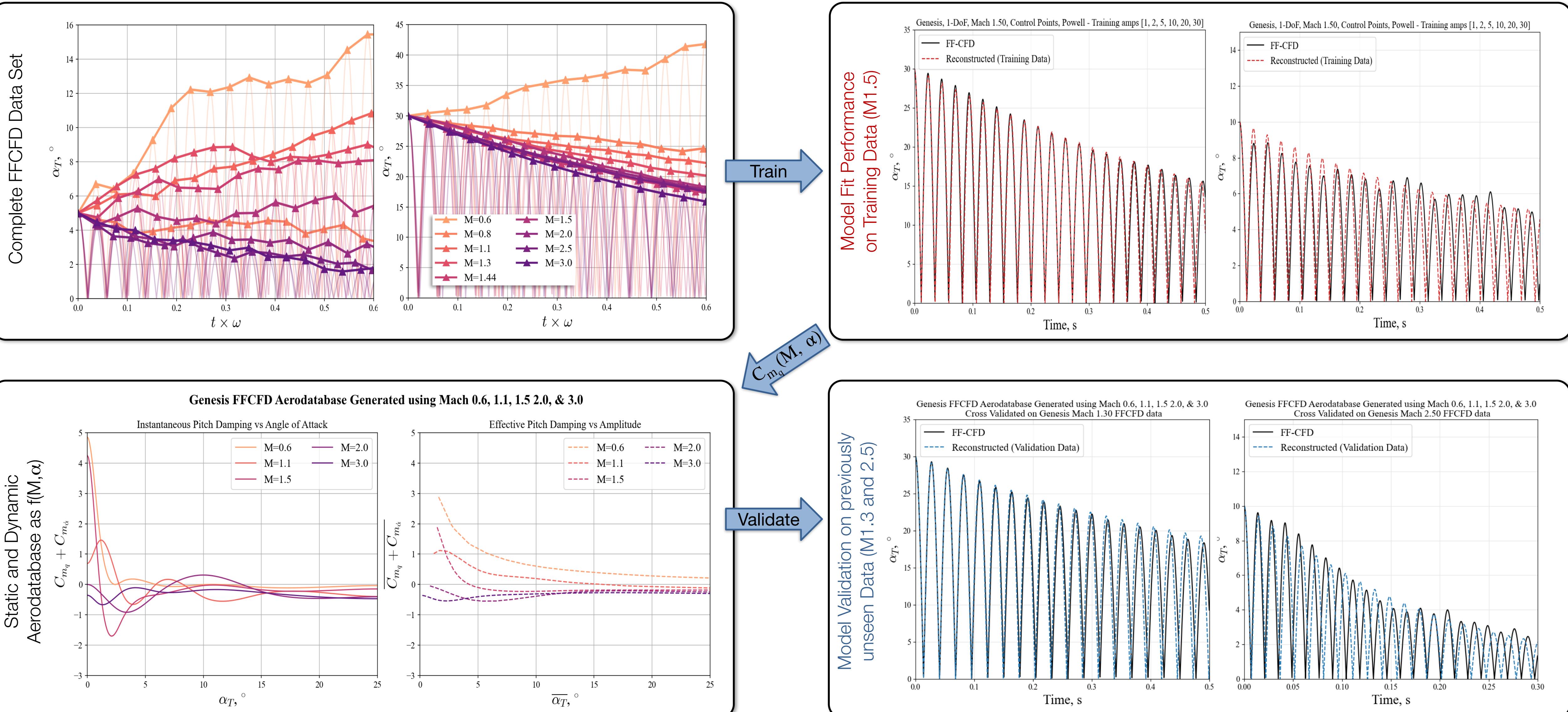
# End-to-End Example



# End-to-End Example

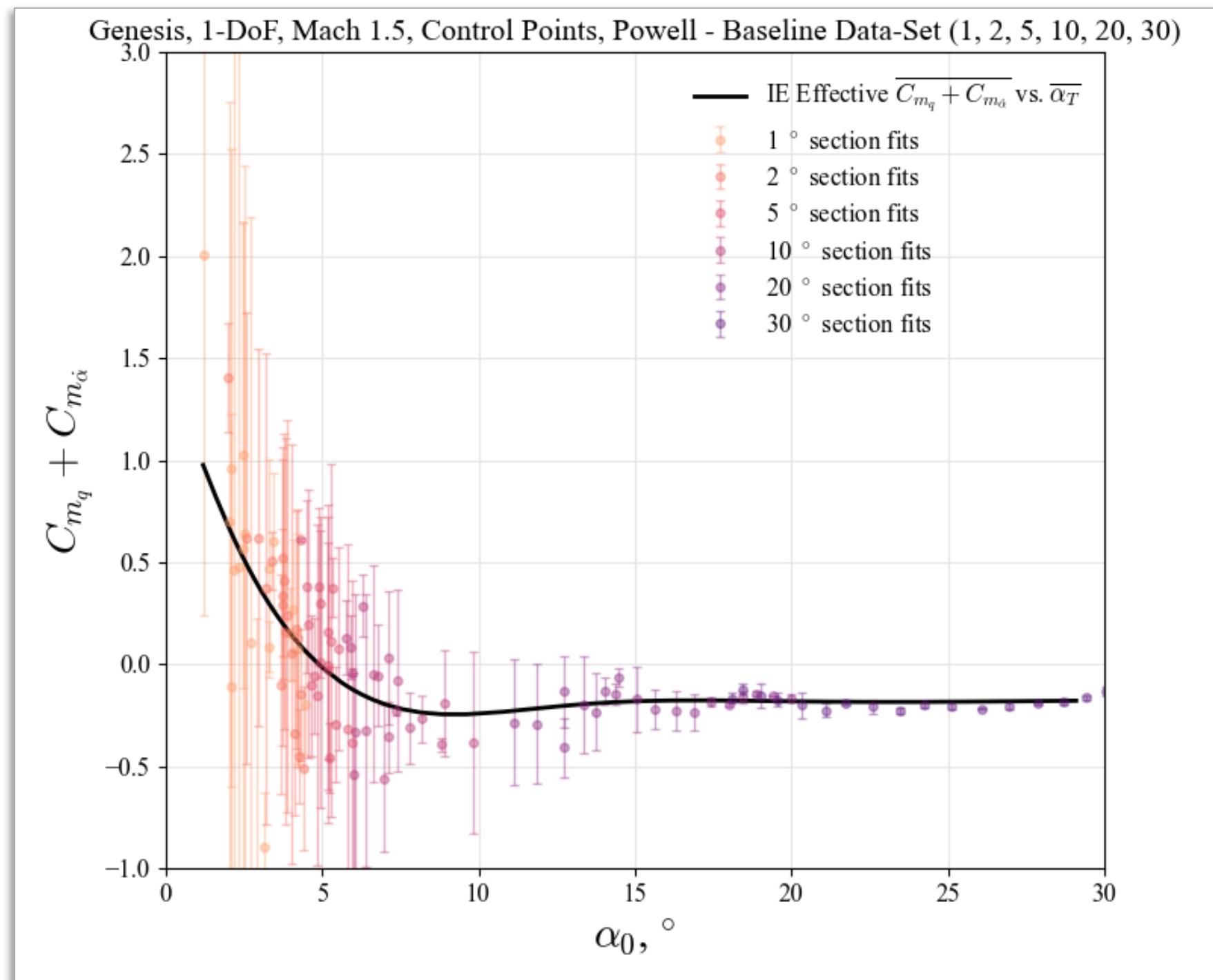


# End-to-End Example

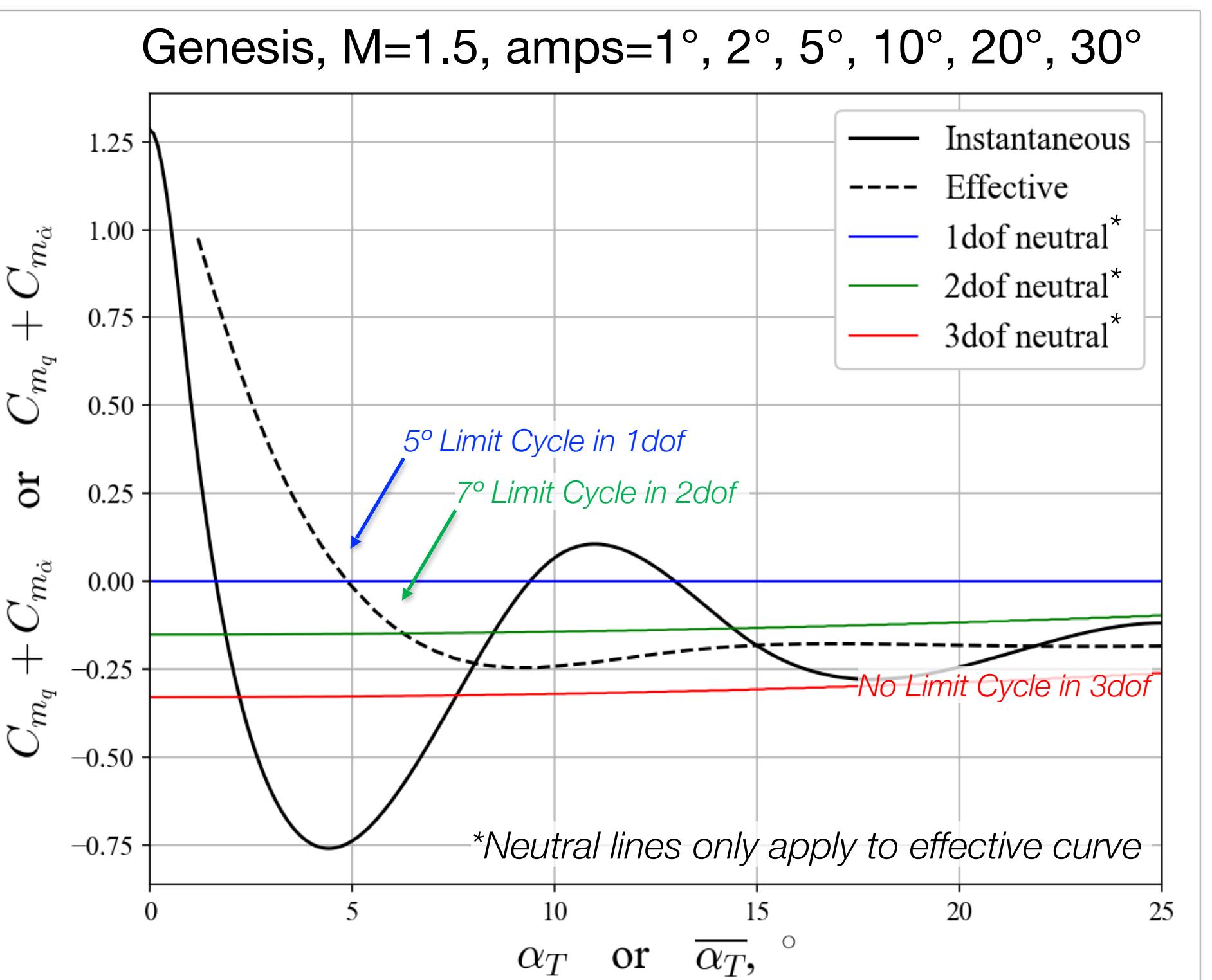


# Utilities: Effective CMq curves, section fits

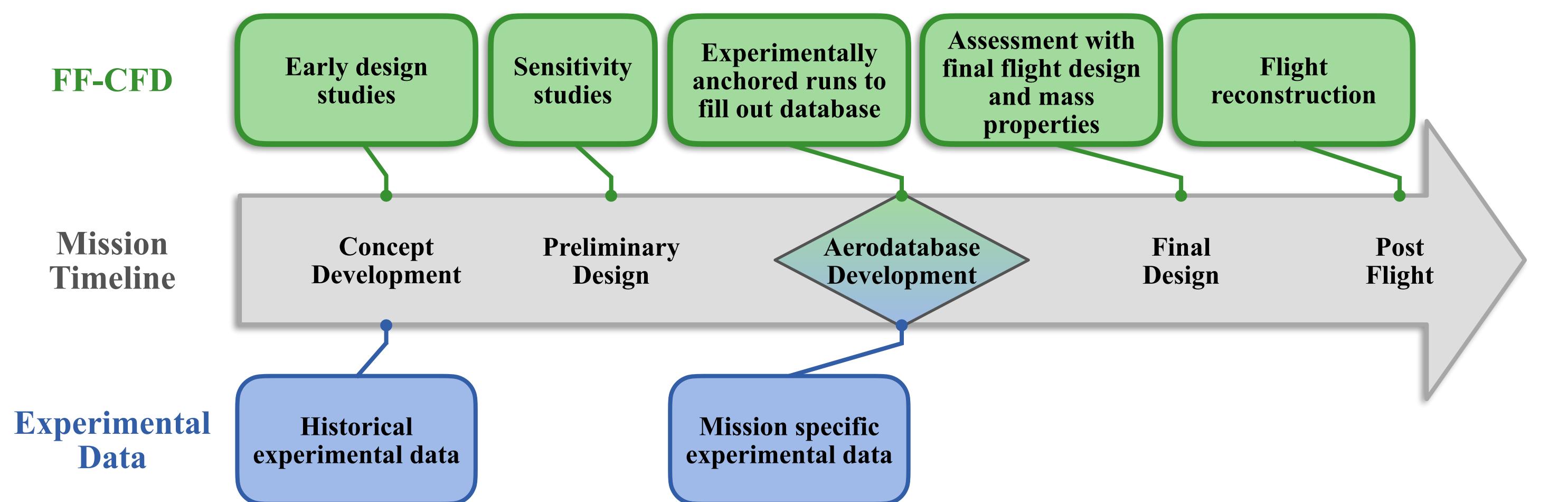
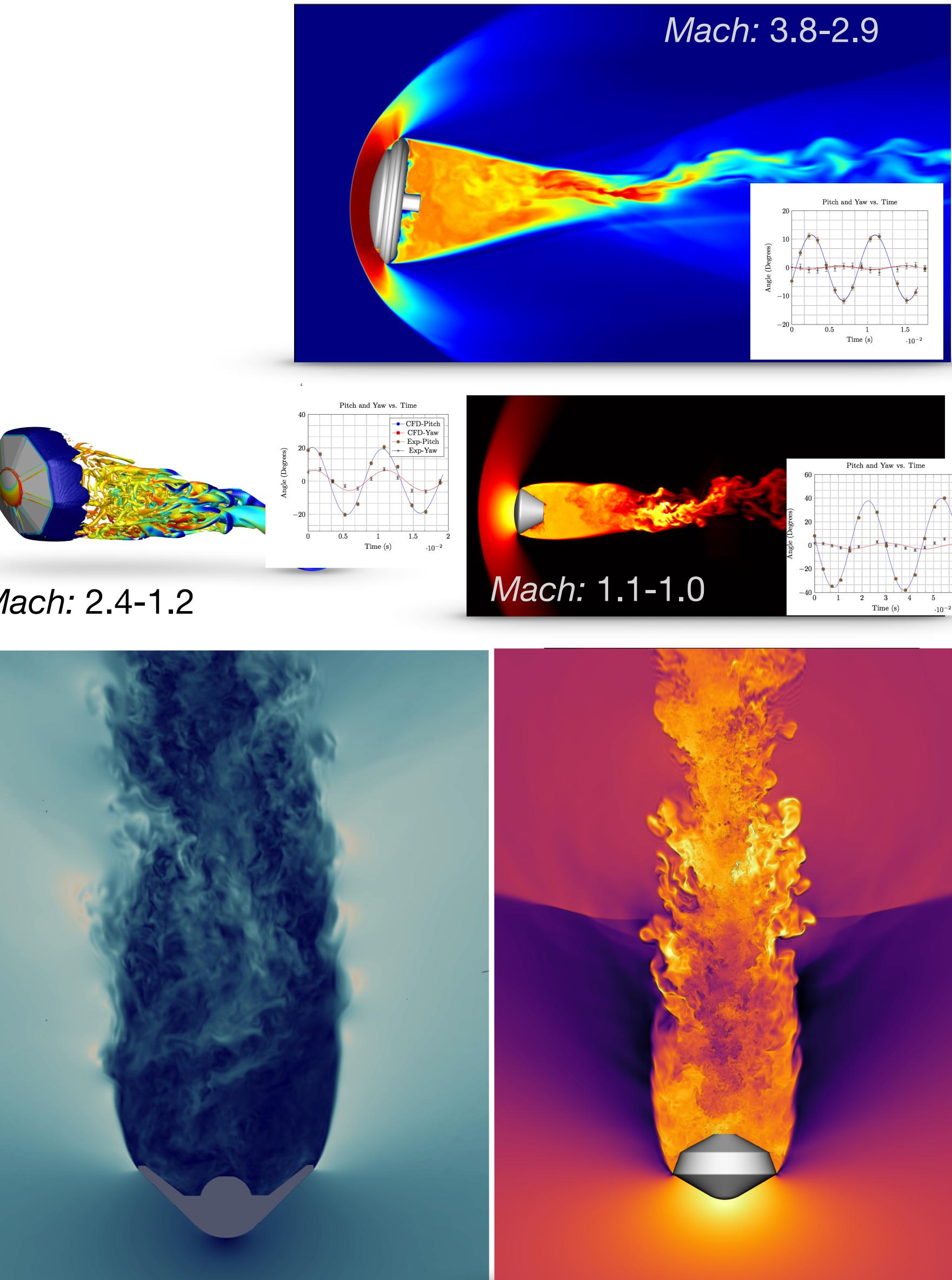
- Effective pitch damping integrated over one cycle
  - Map  $C_{M_q}(\alpha) \rightarrow \bar{C}_{M_q}(\text{amplitude})$
  - $C_{M_q}$  as a function of instantaneous  $\alpha$  is required for integration into flight dynamics simulations
  - Effective  $C_{M_q}$  as a function of oscillation amplitude provides more intuitive insights about where the vehicle is stable and permits more readily digested comparisons between data-sets
  - With effective curve, limit cycle can be predicted for 1dof (simulation or experiment) and 3dof (flight-like) configurations
- Sectional fitting of effective CMq using analytical solutions
  - Shows good agreement with effective CMq curve computed above
  - Provides means to quantify scatter in curve

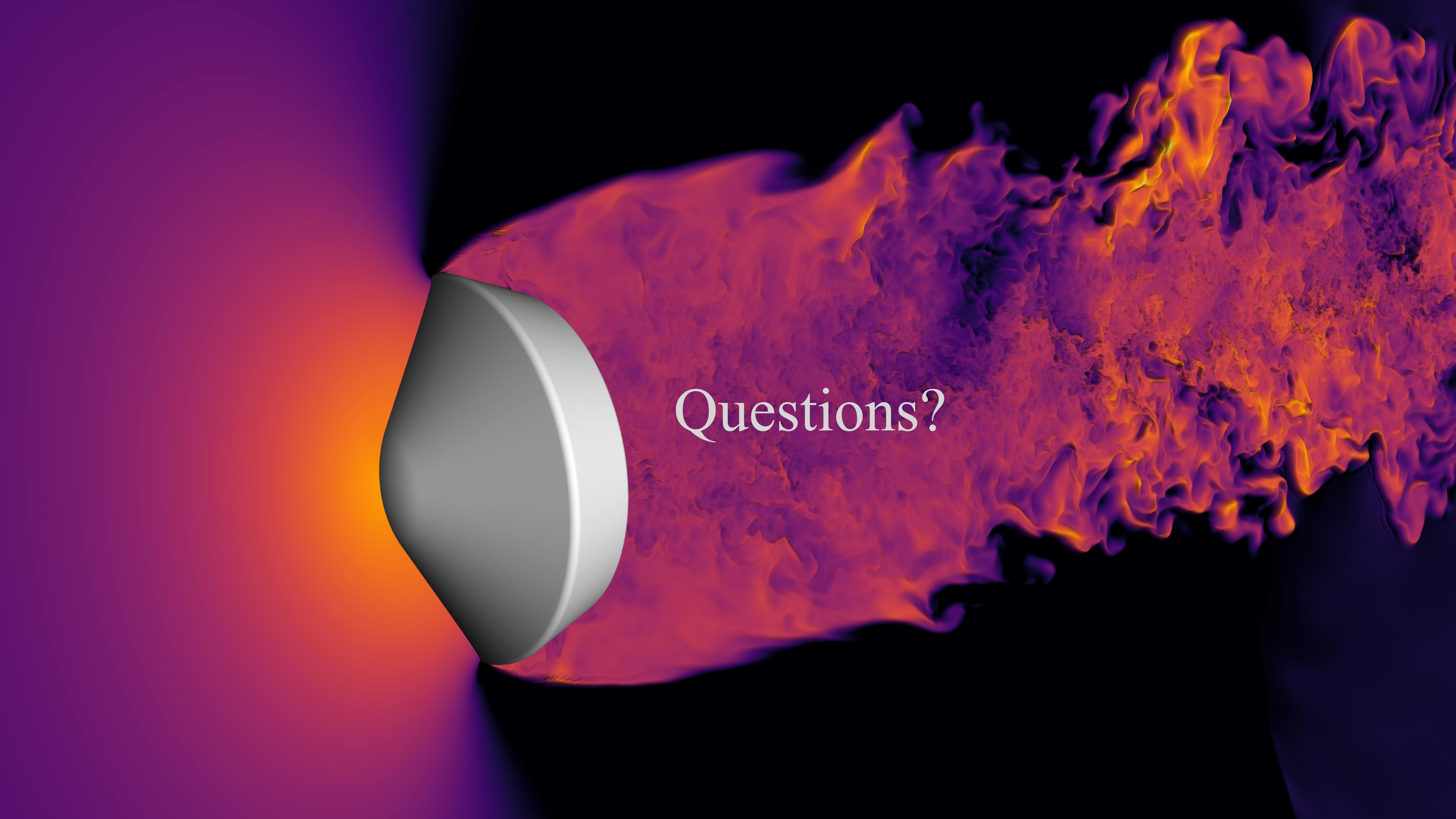


$$\bar{C}_{mq} = \frac{\frac{2\pi}{\omega} \left( C_{mq} + C_{m\dot{\alpha}} \right) \dot{\alpha}^2 dt}{\frac{2\pi}{\omega} \dot{\alpha}^2 dt}$$

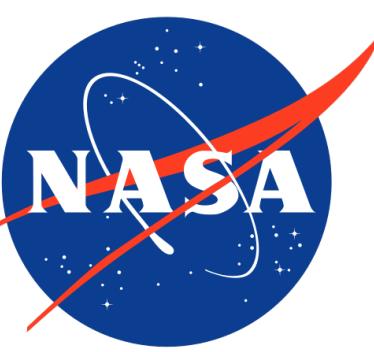


- ESM has invested in Free-Flight CFD capability to bring a computational tool into the portfolio for characterizing dynamic stability
- Extending CFD capability to quantify dynamic stability and perform sensitivity studies for flight projects requires verified and validated tools
  - FF-CFD in US3D has been extensively validated in the supersonic, transonic, and mid-subsonic regime
  - Dynamic simulations provide a new paradigm to simulate as you fly
- Effort in the last 18 months has expanded into developing the data reduction techniques necessary to produce full aerodynamic databases from FF-CFD data
- With a validated tool for modeling the dynamics and an established method for reducing data, computational tools can provide value throughout mission life





Questions?



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